

AS series



STANDARDFIT Worm gearmotors
Imperial Units





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Rossi for You



Innovation

Rossi offers a wide range of **solutions for an evolving industry**, flexible and innovative gearboxes and gearmotors for customer tailored solutions to maximize performance and minimize the total cost of ownership.



High quality, 3 years warranty

Our drive is to innovate and boost operations by manufacturing performing, precise, reliable and high-quality products all over the world. We are always one step forward in offering and developing solutions that can satisfy an unlimited number of application needs, even in the most demanding conditions.



Reliability

We are a reliable company with the right flexibility and know-how to respond to worldwide market requests, in all application fields, without leaving aside our commitment for the environment and value on human safety, to protect everyone's future.



Tools and processes

We continue to invest in new tools and processes, so our highly skilled specialist team in different fields are supporting you to find the best solution suitable for your demands, always by your side on every step of the project.



After-sale service

Highly trained mechanics and support teams can ensure a fast and efficient after-sale service providing support worldwide.



Digital support

Alongside our 24/7 **Rossi for You** support portal you have a suite of digital support tools enabling real time access to your order tracking, invoices, spare part tables download and contact to our service.



Experience

Shaped by more than 60 years of history Rossi meets your unique needs whether you need a standard design or a customized solution.



Global presence local service



Local support

Sales, customer service,
technical support, spare parts



15 branches*



Worldwide distribution network*

A widespread sales network of subsidiaries and dealers in nearly all industrialized countries. By your side from the design to after-sale phase, Rossi is a flexible and dependable partner throughout the world.

Rossi for You, our customer web portal, provides a 24/7 global coordination of the ordering, supply and service processes.

*All contacts available on www.rossi.com



United States

Suwanee, GA

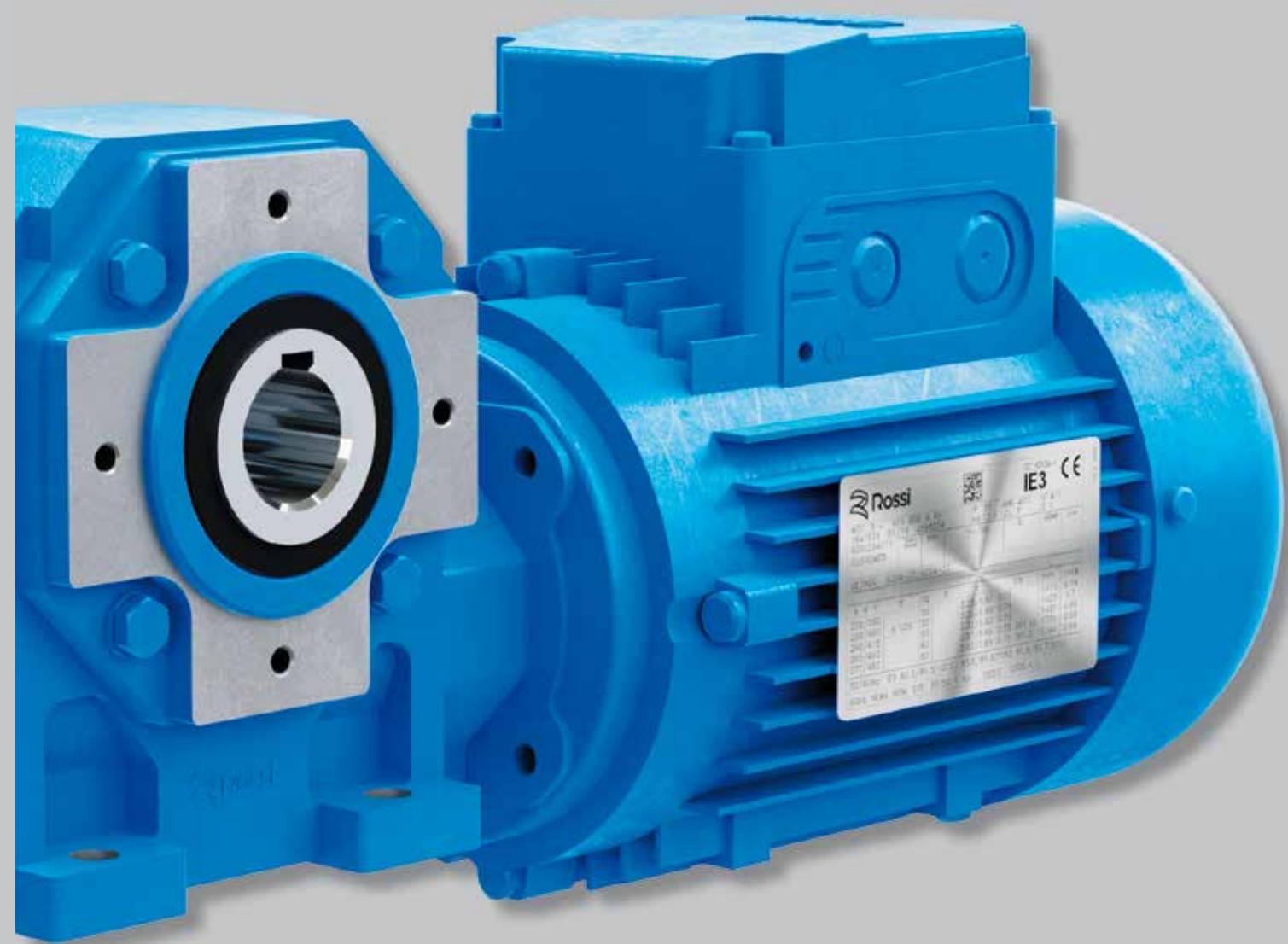


Brazil

Cordeiropolis, SP



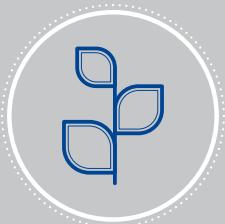
Features, benefits and range





Maximum performance

We drive the heaviest applications
worldwide



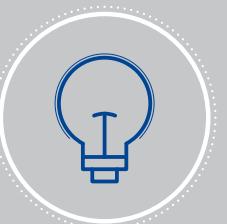
Sustainability

We care
about environment



Modular system

For cost-effective
and high quality solutions



Innovation

We are constantly thinking forward,
solutions for an evolving industry



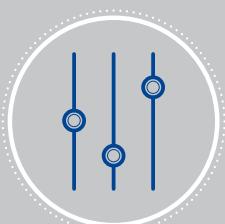
Digitalization

Rossi for You is always at your disposal
for any info



Know-how

We support you through
interdisciplinary know-how



Customization

Cost-effective solutions starting from
standard products

2 - Features, benefits and range

Train of gears:

- worm gear pair;
- **6 sizes** with final reduction center distance to R 10 series;
- nominal transmission ratios to R 10 series (6 ... 75);
- casehardened/hardened cylindrical worm made of 16MnCr5 EN 10084-98 steel with ground and **superfinished involute profile (ZI)**;
- worm-wheel with profile especially conjugate to the worm through hob optimization, with hub in nodular cast iron and **Nibronze CuSn12Ni2-B** (EN1982-98) gear rim with high pureness and controlled phosphor contents;
- train of gear load capacity calculated for breakage and wear; thermal capacity verified.

Specific standards:

- nominal transmission ratios and principal dimensions according to UNI 2016 standard numbers (DIN 323-74, NF X 01.001, BS 2045-65, ISO 3-73);
- basic rack to BS 721-83; involute profile (ZI) to UNI 4760/4-77 (DIN 3975-76), ISO/R 1122/2-69;
- fixing flanges B14 and B5 (the latter with spigot «recess») taken from UNEL 13501-69 (DIN 42948-65, IEC 72.2);
- parallel keys to UNI 6604-69 (DIN 6885 Bl. 1-68, NF E 27.656 and 22.175, BS 4235.1-72, ISO/R 773-69) except for specific cases of motor-to-gear reducer coupling where key height is reduced;
- mounting positions taken from UNEL 05513-67 (DIN 42950-64, IEC 34;7);
- worm gear pair load capacity and efficiency to **BS 721-83** integrated with ISO/CD 14521.

Sound levels

The standard levels of sound power emission L_{WA} relevant to the gearmotors of this catalogu, running at nominal load and speed, fulfil the limits settled by VDI 2159 for gear reducers and EN 60034 for motors.

Asynchronous three-phase motors, brake motors



HB

Asynchronous three-phase motor



HBZ

Asynchronous three-phase **brake motor** with **d.c. brake**



HBF

Asynchronous three-phase **brake motor** with **a.c. brake**



HBV

Asynchronous three-phase **brake motor** with **d.c. safety brake**

2 - Features, benefits and range

Advanced design motors sharing the **same stator windings**, the same **rotors**, the same **housings**, the same **flanges**, the same performance, and the majority of technical solutions with its twin brake motor series (**HBZ, HBF, and HBV**).

The generous electromagnetic sizing allow to achieve **high efficiency values** complying with **different energy saving regulations**:

- Efficiency class **IE3 (ErP)** for HB;
- Efficiency class **IE3 (ErP)** on request for HBZ

The electric design (terminal block, name plate, etc.) has been studied to comply, as standard, also with **NEMA MG1-12** for the maximum application flexibility and facility.

The strength and the precision of mechanical construction, the generous bearings and the wide range of non-standard designs available on catalog make this motor particularly suitable for coupling with gearmotors.

Thanks to its outstanding **low noise, progressivity** and **dynamic** characteristics, it is specifically suitable for **coupling with gearmotor minimizing the dynamic overloads** deriving from **starting and braking phases** (especially in case of motion reversals) and maintaining a **very good braking torque value**.

The excellent **operation progressivity** - when starting and braking - is assured by the brake anchor which is less quick in the impact (compared to a.c. HBF) and by the slight quickness of d.c. brakes.

Offering a comprehensive **range of accessories and non-standard designs** in order to satisfy all possible gearmotor application fields.

The **high reactivity** typical of **a.c. brake** and the **high braking capacity** make this brake motor **particularly suitable for heavy duties** requiring **quick brakings** and a **high number of operations** (e.g.: lifts with high frequency of starting, usually for size > 132, and/or for jog operations).

Vice versa, its very **high dynamic characteristics** (rapidity and frequency of starting) **are not advisable for the use** in **gearmotor** coupling, especially when these features are not strictly necessary for the application (avoiding useless overloads on the whole transmission).

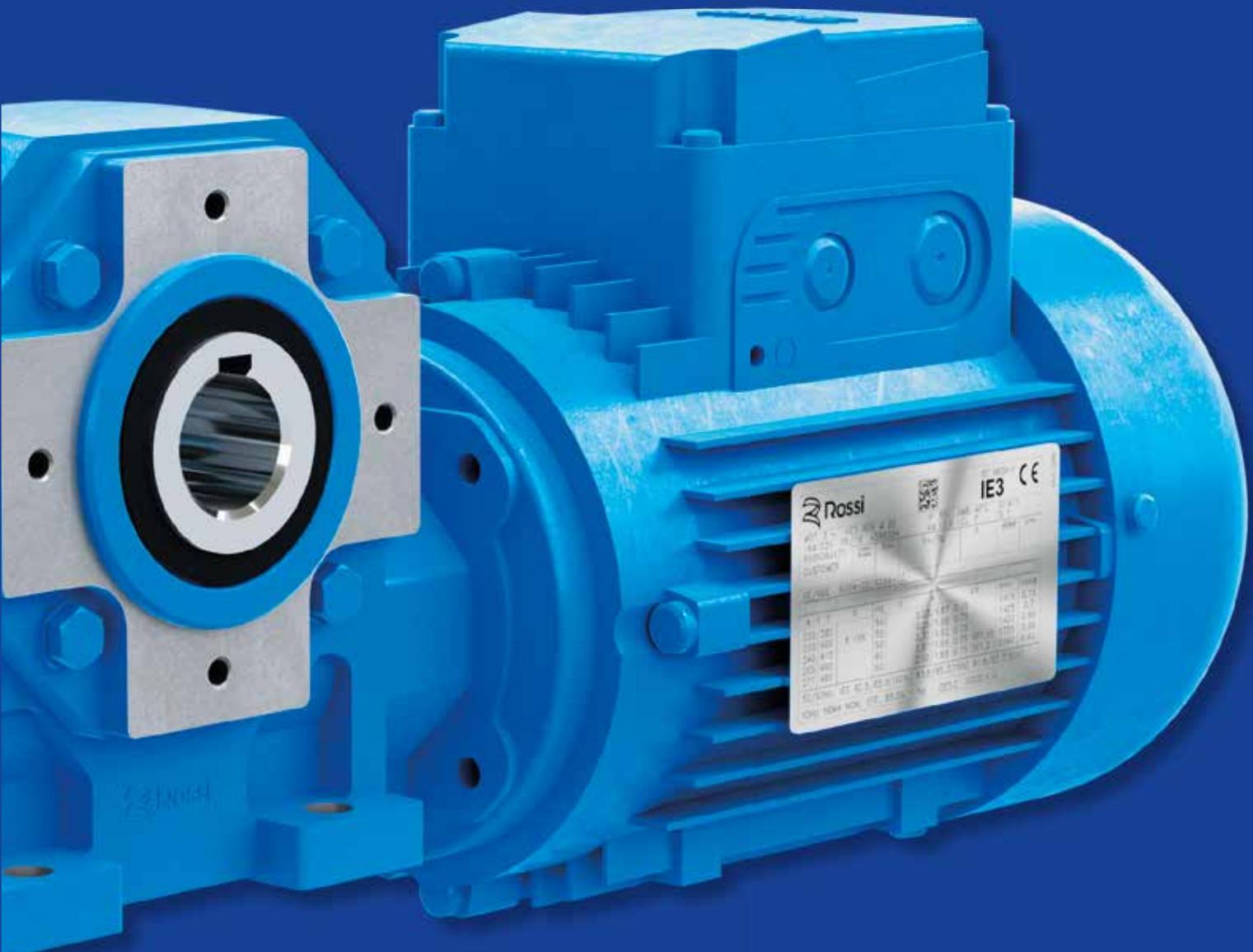
Comprehensive **range of accessories and non-standard designs** in order to satisfy all application needs of gearmotors (in particular for HBF: IP 56, IP 65, encoder, independent cooling fan, independent cooling fan and encoder, double extension shaft, etc.).

Featuring **maximum economy, very reduced overall dimensions and moderate braking torque**, it is suitable for the coupling with gearmotor and can be applied as brake for **safety or parking stops** (e.g. cutting machines) and for operations at deceleration ramp end **during the running with inverter**.

The standard cast iron fan supplies a flywheel effect increasing the very good progressivity of starting and braking (typical of d.c. brake) being particularly **suitable for «light»¹⁾ traverse movements**.

1) Mechanism group M4 (max 180 starts/h) and on-load running L1 (light) or L2 (moderate) to ISO 4301/1, F.E.M./II 1997.

Product overview





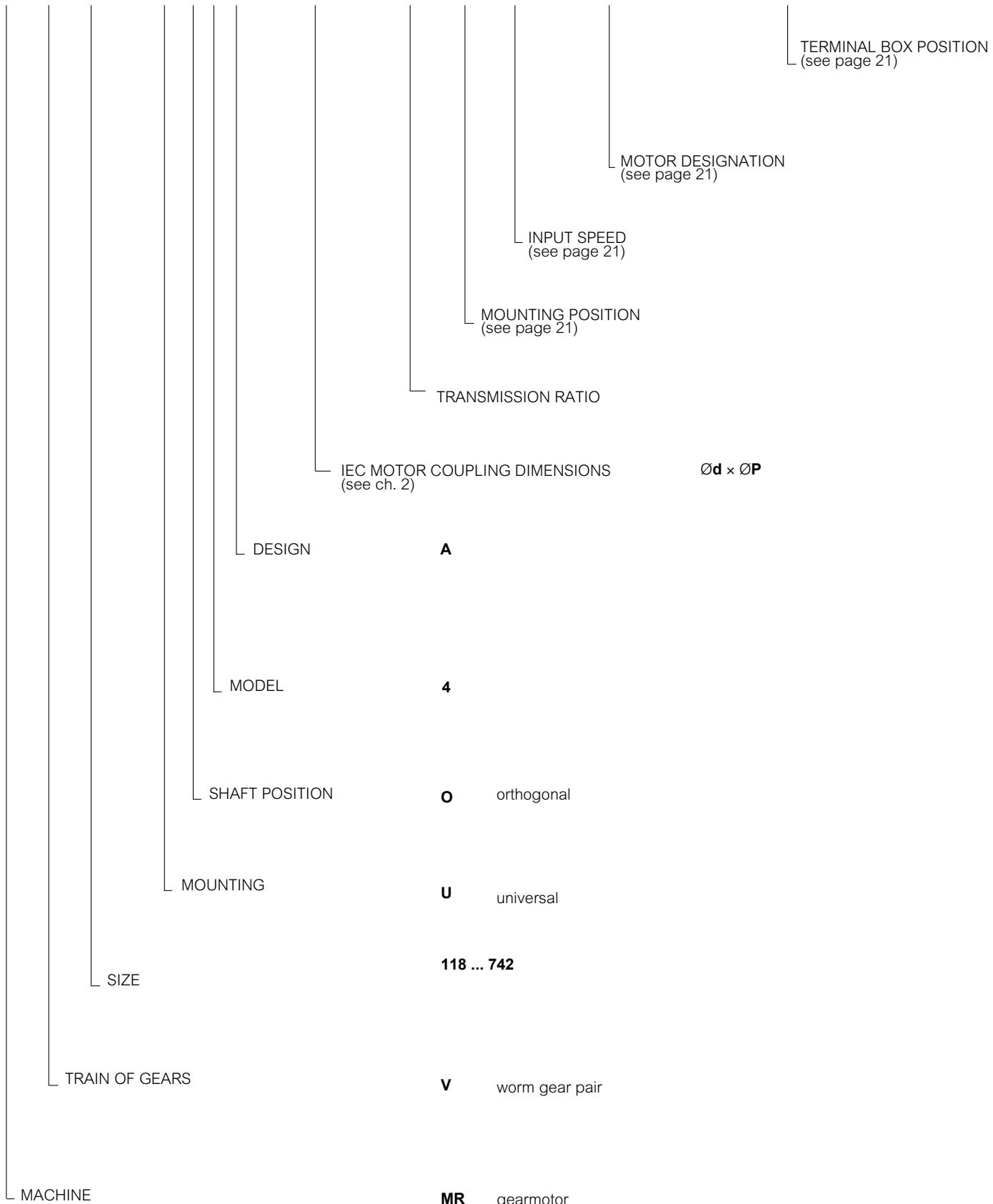
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3.1 - Designation

Designation code

MR V 742 U O 4 A - 28 x 250 - 23,5 V5 HB3 112M4 230.400-50 B5 TB3



3.4 - Service factor f_s

Service factor f_s takes into account the different running conditions (nature of load, running time, frequency of starting, other considerations) to which the gearmotor can be subjected and which must be referred to when performing calculations of gearmotor selection and verification.

Two equivalent methods are here proposed to determine the minimum service factor required by applications:

- **mass acceleration method**: considering the overloads deriving from the system inertia and running conditions (starts per hour, hours per day, expected life);
- **AGMA service factor**, according to AGMA standards (although the gearmotors of the present catalog are not strictly AGMA rated).

Mass acceleration method

For an analitical determination of the required service factor (espe-cially considering the running hours), proceed as stated below and/or consult us

- Calculate the **mass acceleration factor m_j** :

$$m_j = \frac{WK_R^2}{WK_0^2}$$

where:

WK_R^2 [lb ft²] is the external moment of inertia (of mass; couplings, driven machine)

WK_L^2 reflected to the motor shaft:

$$WK_R^2 = WK_L^2 \cdot \left(\frac{n_2}{n_N} \right)^2$$

WK_L^2 [lb ft²] is the moment of inertia (of mass) of motor (see ch. 2b);

n_2 [rpm] is output speed of the gearmotor;

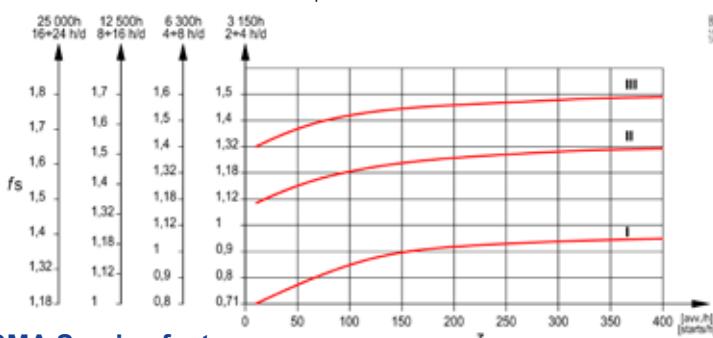
n_N [rpm] is nominal speed of the motor (see ch. 2b). As a guideline consider: $n_N = 1\,750$ rpm for 4 poles and $n_N = 1\,150$ rpm for 6 poles;

- Select the proper **overload class** according to the acceleration mass factor m_j :

$m_j \leq 0.3$	(uniform load)	load classification I
$m_j \leq 3$	(moderate overloads)	load classification II
$m_j \leq 10$	(heavy overloads)	load classification III

For m_j values larger than **10**, in presence of high values of backlash for kine-matic chain, a specific evalutation has to be carried out: consult us.

- From the **diagram**, according to the overload class, the running time and the starting frequency z , read off the minimum service factor required.



Whenever a **higher reliability degree** is required for the application (e.g.: personnel safety, key importance of the gearmotor to production, particularly difficult maintenance conditions, etc.) multiply f_s by **1,25** ÷ **1,4**: consult us.

AGMA Service factor

Service factor

For a proper selection olf gearmotor service factor, the magnitude and duration of shock loads, the duration of service per hour, per day, and per week, as well as the required reliability must be determined.

Although the gearmotors of the present catalog are not stricly AGMA rated, nevertheless the following table (gear reducer driven by an electric motor) can be used to select a proper service factor as well.

It is recommended that service factor for unique applications be agreed upon by the end user and the manufacturer.

The following discussion of shock loads and duration of service are provided as a guide to proper classification of applications.

Load classification

Since the gearmotor rating applies to applications involving uniform loads, the magnitude of any recurrent shock loads should be estimated or determined through test by the system designer. The loading conditions may be classified as follows:

- **uniform load**. Recurrent shock loads do not exceed the **nominal** specified input power;
- **moderate shock load**. Recurrent shock loads do not exceed **125** percent of the nominal specified input power;
- **heavy shock load**. Recurrent shock loads do not exceed **150** percent of the nominal specified input power;
- **extreme shock load**. Recurrent shock loads do not exceed **175** percent of the nominal specified input power.

Duration [hours per day]	Service factor			
	Uniform load	Moderate shock	Heavy shock	Extreme shock
Occasional 1/2 hour	(0.75) ¹	(0.90) ¹	1.00	1.25
≤ 3	1.00	1.00	1.25	1.50
3 - 10	1.00	1.25	1.50	1.75
> 10	1.25	1.50	1.75	2.00

¹) These service factors should be 1.00 or as agreed by the user and the manufacturer.

Caution: in case of high reliability degree requirements (e.g.: application involving risks for personnel safety) or in presence of high inertia loads or high starts/stops frequency, consult us.

3.5 - Selection

Determining the gearmotor size

- Make available all necessary data: required output power P_2 of gearmotor, speed n_2 , running conditions (nature of load, running time, frequency of starting z, other considerations) with reference to ch. 3.4.
- Determine service factor f_s on the basis of running conditions (ch. 3.4).
- Select the gearmotor size on the basis of n_2 , f_s , P_2 (ch. 3.7).

When for reasons of motor standardization, power P_2 available in catalogue is much greater than the power P_2 required, the gearmotor can be selected on the basis of a lower service factor provided,

$$\left(f_s \cdot \frac{P_2 \text{ required}}{P_2 \text{ available}} \right)$$

it is certain that this excess power

available will never be required and frequency of starting z is low enough not to affect service factor (ch. 3.4).

Calculations can also be made on the basis of torque instead of power; this method is even preferable for low n_2 values.

Verifications

- Verify possible radial load F_{r2} referring to directions and values given in ch. 3.6 and 3.7.
- For the motor, verify frequency of starting z when higher than that normally permissible, referring to directions and values given in ch. 2 cat. TX; this will normally be required for brake motors only.
- When load chart is available, and/or there are overloads – due to starting on full load (especially with high inertias and low transmission ratios), braking, shocks, irreversible or with low reversibility gear reducers in which the worm-wheel becomes driving member due to the driven machine inertia, other static or dynamic causes – verify that the maximum torque peak (ch. 3.9) is always less than $T_{2\max}$ (indicated in ch. 3.7); if it is higher or cannot be evaluated – in the above instances – install suitable safety devices so that $T_{2\max}$ will never be exceeded.
- In general, thermal power verification (ch. 3.3) is not required for the combinations foreseen in ch.3.7, exception made for those cases indicated by * or ** for which:
 - * thermal power verification is necessary if, for continuous duty, the **ambient temperature is > 86 °F (30 °C)** or running is in **full power**;
 - ** thermal power is **always** to be verified.

Considerations on selection

Motor power

Taking into account the efficiency of the gear reducer, and other drives – if any – motor power is to be as near as possible to the power rating required by the driven machine: accurate calculation is therefore recommended.

The power required by the machine can be calculated, seeing that it is related directly to the power-requirement of the work to be carried out, to friction (starting, sliding or rolling friction) and inertia (particularly when mass and/or acceleration or deceleration are considerable). It can also be determined experimentally on the basis of tests, comparisons with existing applications, or readings taken with amperometers or wattmeters.

An oversized motor would involve: a greater starting current and consequently larger fuses and heavier cable; a higher running cost as power factor ($\cos \phi$) and efficiency would suffer; greater stress on the drive, causing danger of mechanical failure, drive being normally proportionate to the power rating required by the machine, not to motor power.

Only high values of ambient temperature, altitude, frequency of starting or other particular conditions require an increase in motor power.

Driving machines with high kinetic energy

In presence of driving machines with high inertias and/or speeds, avoid the use of irreversible gearmotors as stopping and braking can cause very high overloads (ch. 3.9).

3.6 - Radial loads (overhung loads OHL) F_{r2} [lbf] on low speed shaft end

Radial loads generated on the shaft end by a drive connecting gearmotor and machine must be less than or equal to those given at ch. 3.7.

Normally, radial loads on low speed shaft end are considerable: in fact there is a tendency to connect the gear reducer to the machine by means of a transmission with high transmission ratio (economizing on the gear reducer) and with small diameters (economizing on the drive, and for requirements dictated by overall dimensions).

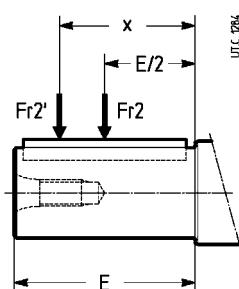
Bearing life and wear (which also affects gears unfavourably) and low speed shaft strength, clearly impose limits on permissible radial load.

Permissible radial loads are given in the tables of ch. 3.7 and are referred to gearmotor's output speed n_2 and torque T_2 , considering overhung load acting on centre line of standard low speed shaft end (see ch. 4), in the most unfavourable direction of rotation and angular position of load.

If the exact direction of rotation and angular position of load are known, an increase of permissible radial load may be achieved. If necessary, consult us for the verification of specific instance.

In case of radial load acting in position different from centre line of low speed shaft end, i.e. operating at a distance different from $0.5 \cdot E$, the permissible radial load must be recalculated according to the following formula, verifying not to exceed $F_{r2\max}$ max value stated in the table:

$$F_{r2}' = F_{r2} \cdot \frac{E/2 + k}{x + k} \quad [\text{lbf}]$$



Where:

- F_{r2}' [lbf] is the permissible radial load acting at the distance x from shaft shoulder;
- F_{r2} [lbf] is the permissible radial load acting on centre line of standard low speed shaft end (see ch. 3.7);
- E [in] is standard low speed shaft end length (see following table and ch. 5);
- k [in] is given in the table;
- x [in] is the distance between the shaft shoulder and the load application point.

	Gear reducer size					
	118	225	325	430	535	742
E [in]	1.1	1.6	1.6	2.2	2.2	3.2
k [in]	2.05	2.58	3.05	3.68	4.35	5.24
$F_{r2\max}$ [lbf]	450	600	900	1 250	1 450	1 700

An **axial load** of up 0.2 times the value in the tables of ch. 3.7 is permissible, simultaneously with the radial load.

In case of no radial loads an axial load (not misaligned) of up 0.5 times the value in the tables of ch. 3.7, is permissible. For higher values and/or **misaligned** axial loads, consult us.

Radial load F_{r2} for most common drives has the following value:

$$F_{r2} = k \cdot \frac{2 \cdot T_2}{d} \quad [\text{N}]$$

where:

T_2 [lbf in] is the torque required by the gearmotor low speed shaft;
 d [in] is the pitch diameter;

k is a coefficient which assumes different values according to transmission type:

$k = 1$ for chain drive (lifting in general);

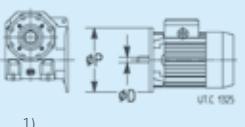
$k = 1.5$ for timing belt drive;

$k = 2.5$ for V-belt drive;

$k = 1.1$ for spur gear pair drive;

$k = 3.55$ for friction wheel drive.

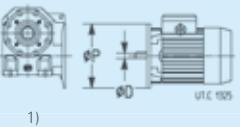
3.7 - Selection tables

Motor power	Output speed	Output power	Output torque	Max output torque	OHL	Service factor	fs	1)		2)	HB	HBz
		P ₁ hp	n ₂ rpm	P ₂ hp	T ₂ lbf in	T _{2max} lbf in	F _{r2} lbf	i				
0,25	39,8 50 62,5 79,5 103 125 159 206 292	0,17 0,18 0,19 0,19 0,2 0,21 0,21 0,22 0,22	270 225 190 155 120 105 84 66 47,9	370 400 435 465 420 405 420 370 335	400 425 375 335 315 265 236 212 180	44 35 28 22 17 14 11 8,5 6	0,8 1,12 1,4 1,9 2,12 2,36 2,8 3,15 4		MR V 118 - 11 x 90 63 B 4 B14	6,8	16,5	21
0,33	19,8 24,5 30,3 38,3 24 30,2 37,2 46,1 58,3 72,9 92,1	0,22 0,23 0,24 0,25 0,22 0,23 0,24 0,25 0,26 0,26 0,28	695 590 500 410 570 480 405 340 280 230 190	1200 1470 1670 1740 850 1180 1310 1490 1560 1430 1410	900 800 750 630 850 800 670 600 560 560 500	58 47 38 30 73 58 47 38 30 24 19	1,18 1,6 2,12 2,65 1,12 1,6 2 2,65 3,35 3,75 4,5		MR V 325 - 14 x 105 71 B 6 B14	14	29	35
									MR V 325 - 14 x 105 71 A 4 B14	14	27	33
	30,3 38,3 47,9	0,23 0,24 0,25	485 400 330	865 945 855	600 530 530	38 30 24	1,12		MR V 225 - 11 x 90 71 B 6 B14R	8,6	24	30
	37,2 46,1 58,3 72,9 92,1	0,24 0,25 0,25 0,26 0,28	400 335 275 225 190	685 765 820 760 715	560 500 450 425 355	47 38 30 24 19	1,06		MR V 225 - 11 x 90 63 C 4 B14	8,6	20	24
	37,2 46,1 58,3 72,9 92,1 113 146	0,24 0,25 0,25 0,26 0,28 0,28 0,28	400 335 275 225 190 155 125	685 765 820 760 715 755 665	560 500 450 425 355 335 300	47 38 30 24 19 15,5 12	1,06		MR V 225 - 11 x 90 71 A 4 B14R	8,6	21	27
	41,1 52,3 67,6 82,1	0,23 0,24 0,25 0,27	360 295 235 205	495 530 475 465	425 425 400 335	28 22 17 14	0,85 1,12 1,32 1,5		MR V 118 - 11 x 90 71 B 6 B14R	6,8	22	28
	50 62,5 79,5 103 125 159	0,24 0,25 0,25 0,26 0,28 0,28	300 250 200 160 140 110	400 435 465 420 405 420	375 375 375 335 280 224	35 28 22 17 14 11	0,85		MR V 118 - 11 x 90 63 C 4 B14	6,8	18	22
	50 62,5 79,5 103 125 159 206 292	0,24 0,25 0,25 0,26 0,28 0,28 0,28 0,29	300 250 200 160 140 110 87 63	400 435 465 420 405 420 370 335	375 375 375 335 280 224 200 180	35 28 22 17 14 11 8,5 6	0,85		MR V 118 - 11 x 90 71 A 4 B14R	6,8	19,5	25

1) For complete designation when ordering see ch. 3.1.

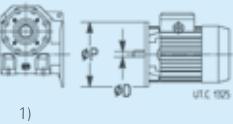
2) Values valid for gearmotor without motor.

3.7 - Selection tables

Motor power	Output speed	Output power	Output torque	Max output torque	OHL	Service factor			1)					
										2)	HB	HBZ		
0,5	15,8 19,8 24,5	0,34 0,36 0,37	1360 1140 960	3440 4820 5170	1500 1500 1500	73 58 47	1,7 2,5 3,35	MR V 535 - 19 x 200	80 A	6	B5	45	63	71
	15,8 19,8 24,5 31,1 38,3 47,9	0,32 0,34 0,36 0,37 0,38 0,39	1280 1080 920 750 630 520	1700 2340 2660 3020 3170 3060	1250 1250 1060 950 900 850	73 58 47 37 30 24	0,95 1,32 1,8 2,5 3,15 3,75	MR V 430 - 19 x 200	80 A	6	B5	25	43	51
	24,5 30,3 38,3 47,9	0,35 0,36 0,38 0,39	890 755 620 510	1470 1670 1740 1620	800 800 630 630	47 38 30 24	1,06 1,4 1,8 2	MR V 325 - 14 x 105	71 C	6	B14	14	31	37
	30,2 37,2 46,1 58,3 72,9 92,1 113 146	0,35 0,36 0,38 0,39 0,4 0,42 0,43 0,43	730 615 515 425 345 290 240 190	1180 1310 1490 1560 1430 1410 1400 1280	800 750 630 530 500 475 450 400	58 47 38 30 24 19 15,5 12	1,06 1,32 1,8 2,24 2,5 3 3,35 4	MR V 325 - 14 x 105	71 B	4	B14	14	29	35
	38,3 47,9	0,37 0,38	605 500	945 855	530 530	30 24	0,95 1,06	MR V 225 - 11 x 90	71 C	6	B14R	8,6	25	32
	46,1 58,3 72,9 92,1 113 146 210	0,37 0,39 0,4 0,42 0,42 0,43 0,44	510 415 340 285 235 185 135	765 820 760 715 755 665 625	500 500 475 400 355 315 250	38 30 24 19 15,5 12 8,33	0,95 1,18 1,4 1,6 1,8 2,12 2,65	MR V 225 - 11 x 90	71 B	4	B14R	8,6	23	29
	67,6	0,38	355	475	355	17	0,85	MR V 118 - 11 x 90	71 C	6	B14R	6,8	24	30
	79,5 103 125 159 206 292	0,39 0,4 0,42 0,42 0,43 0,44	305 240 210 170 130 96	465 420 405 420 370 335	355 335 300 250 212 180	22 17 14 11 8,5 6	0,95 1,06 1,18 1,4 1,6 2	MR V 118 - 11 x 90	71 B	4	B14R	6,8	21	27
0,75	15,8 19,8 24,5	0,51 0,54 0,56	2040 1710 1440	3440 4820 5170	1500 1500 1320	73 58 47	1,12 1,7 2,24	MR V 535 - 19 x 200	80 B	6	B5	45	66	75
	24 30,2 37,2 47,3	0,54 0,56 0,58 0,59	1410 1170 985 790	3390 4160 4480 5130	1320 1250 1250 1180	73 58 47 37	1,5 2,36 2,8 4	MR V 535 - 19 x 200	80 A	4	B5	45	62	70
	19,8 24,5 31,1 38,3 47,9	0,51 0,54 0,56 0,58 0,59	1630 1380 1130 945 775	2340 2660 3020 3170 3060	1250 1180 1060 850 800	58 47 37 30 24	0,9 1,18 1,7 2,12 2,5	MR V 430 - 19 x 200	80 B	6	B5	25	46	55

1) For complete designation when ordering see ch. 3.1.
 2) Values valid for gearmotor without motor.

3.7 - Selection tables

Motor power P₁ hp	Output speed n₂ rpm	Output power P₂ hp	Output torque T₂ lbf in	Max output torque T_{2max} lbf in	OHL	Service factor	i	f_S	 1)		2)	HB	HBZ	
7,5	**	60,5	6,4	6710	10600	1250	19	1	MR V 742 - 28 x 250 132 MB 6 B5R		68	196	222	
	**	74,2	6,5	5540	9700	1250	15,5	1,06						
	*	98,3	6,7	4280	10100	1180	11,7	1,4						
	*	139	6,8	3080	8420	850	8,25	1,7						
	*	92,1	6,6	4490	9010	1250	19	1,25	MR V 742 - 28 x 250 112 MC 4 B5		68	141	161	
	*	113	6,6	3700	7980	1250	15,5	1,32						
	*	150	6,8	2840	8510	1060	11,7	1,7						
	*	212	6,9	2040	7030	850	8,25	2	MR V 742 - 28 x 250 132 M 4 B5R		68	196	220	
	*	92,1	6,6	4490	9010	1250	19	1,25						
	*	113	6,6	3700	7980	1250	15,5	1,32						
	**	150	6,8	2840	8510	1060	11,7	1,7						
	**	212	6,8	2040	7030	850	8,25	2						
	**	150	6,7	2820	4710	600	11,7	1	MR V 535 - 24 x 200 112 MC 4 B5R		45	118	138	
	**	212	6,8	2030	3980	530	8,25	1,18						

* On continuous duty with ambient temperature > 86° F (30 °C) or with full load running, thermal power verification is necessary.

** Thermal power is to be verified.

 Motor (cat.TX) with efficiency value not complying with EISA Premium Efficiency class range.

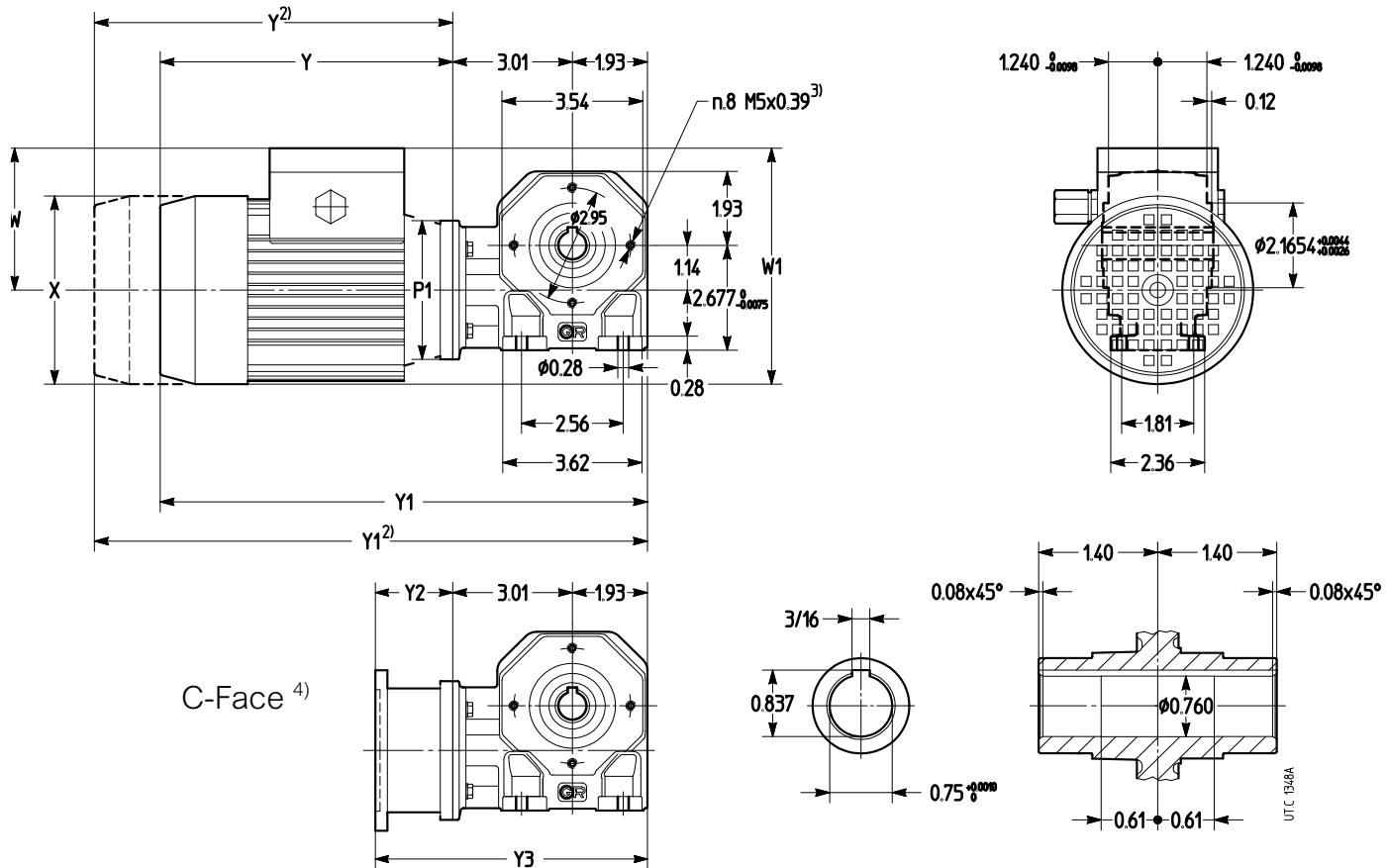
Nominal power and nameplate data refer to intermittent duty S3 70%.

1) For complete designation when ordering see ch. 3.1.

2) Values valid for gearmotor without motor.

3.8 - Dimensions

Size **118**



Motor size 1)	P1 \varnothing	X \varnothing \approx	Y \approx 2)	Y1 \approx 2)	W \approx	W1 \approx	NEMA C-Face adapter ⁴⁾		
							Y2	Y3	
63 B14	90	4.84	7.44	9.61	12.4	14.57	3.74	6.18	MPN 63 B14 - 56 ⁵⁾
71 B14R		5.43	8.5	10.94	13.46	15.91	4.41	7.13	MPN 63 B14 - 56 ⁵⁾

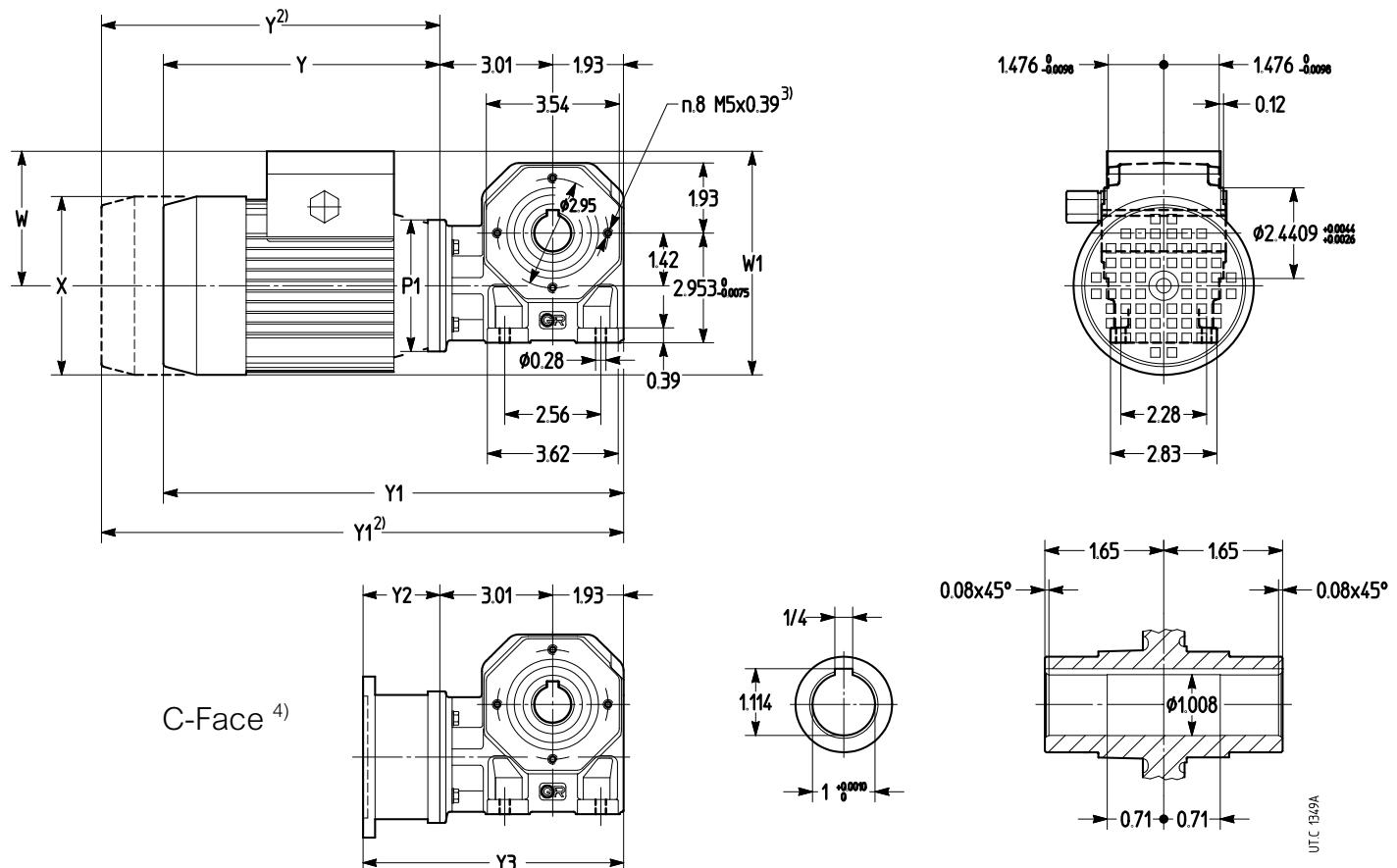
1) Motor mounting position (see ch. 2b).

2) Values valid for HBZ brake motor.

3) No. 4 holes for each of the 2 B14 output flanges.

4) Available on request: for further dimensions and details see ch. 4.

5) Not available for 63B 6 motor.



Motor size 1)	P1 \varnothing	X \varnothing \approx	Y \approx 2)	Y1 \approx 2)	W \approx	W1 \approx	NEMA C-Face adapter ⁴⁾			Y2	Y3
63 B14	90	4.84	7.44	9.61	12.4	14.57	3.74	6.18	MPN 63 B14 - 56 ⁵⁾	2.70	7.64
71 B14R		5.43	8.5	10.94	13.46	15.91	4.41	7.13	MPN 63 B14 - 56 ⁵⁾		

1) Motor mounting position (see ch. 2b).

2) Values valid for HBZ brake motor.

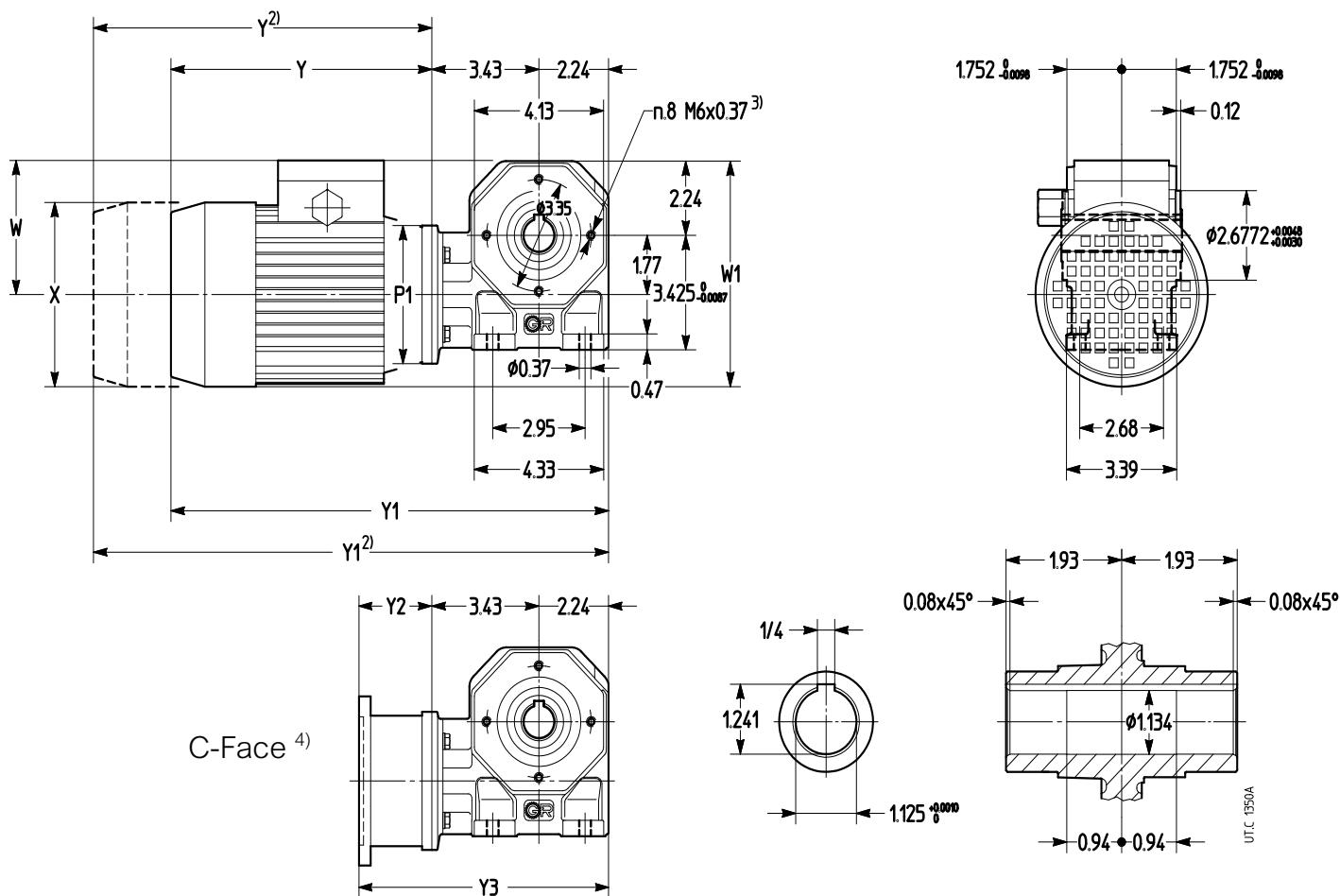
3) No. 4 holes for each of the 2 B14 output flanges.

4) Available on request: for further dimensions and details see ch. 4.

5) Not available for 63B 6 motor.

3.8 - Dimensions

Size **325**



Motor size	P1 Ø ≈	X Ø ≈	Y ≈ 2)	Y1 ≈ 2)	W ≈	W1 ≈	NEMA C-Face adapter ⁴⁾		
							Y2	Y3	
71 B14	105	5.43	8.5	10.94	14.17	16.61	4.41	7.13	MPN 63 B14 - 56 C
80 B14R		6.14	9.17	11.89	14.84	17.56	4.76	7.83	MPN 63 B14 - 56 C

1) Motor mounting position (see ch. 2b).

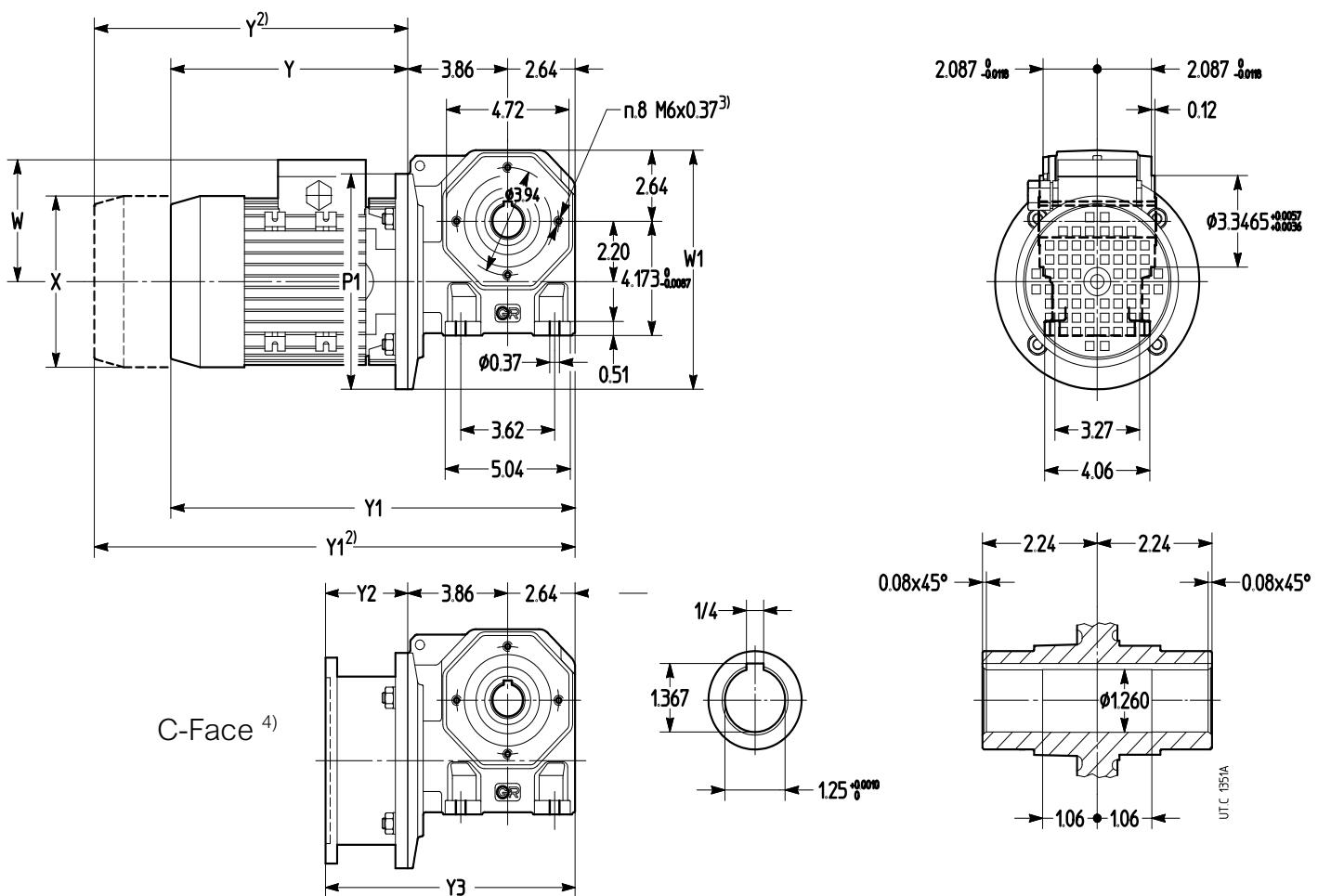
2) Values valid for HBZ brake motor.

3) No. 4 holes for each of the 2 B14 output flanges.

4) Available on request: for further dimensions and details see ch. 4.

3.8 - Dimensions

Size **430**



Motor size 1)	P1 Ø	X Ø ≈	Y ≈ 2)	Y1 ≈ 2)	W ≈	W1 ≈	NEMA C-Face adapter ⁴⁾		
							Y2	Y3	
80 B5	200	6.14	9.17	11.89	15.67	18.39	4.76	8.78	MPN 80 B5 - 56 C
90 L B5R		6.93	11.3	14.41	17.8	20.91	5.55	9.49	MPN 90 B5R - 140 TC
LB B5R									
LC B5R									

1) Motor mounting position (see ch. 2b).

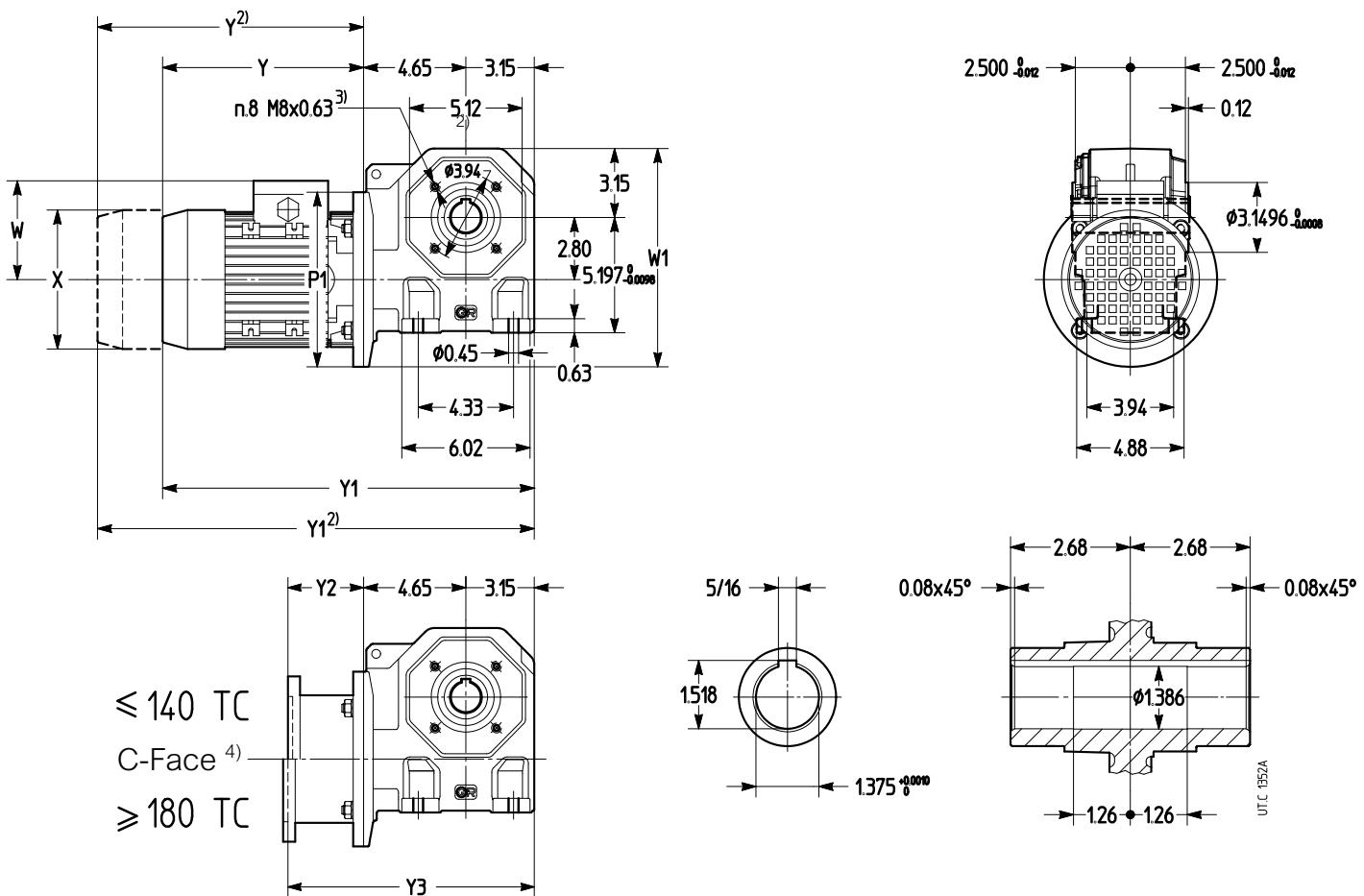
2) Values valid for HBZ brake motor.

3) No. 4 holes for each of the 2 B14 output flanges.

4) Available on request: for further dimensions and details see ch. 4.

3.8 - Dimensions

Size **535**



Motor size 1)	P1 \varnothing \approx	X \varnothing \approx	Y \approx 2)	Y1 \approx 2)	W \approx	W1 \approx	NEMA C-Face adapter ⁴⁾		
							Y2	Y3	
80 B5	200	6.14	9.17	11.89	16.97	4.76	9.88	MPN 80 B5 - 56 C	2.7
90 S B5 L B5 LB B5 LC B5		6.93	11.3	14.41	19.09	5.55		MPN 90 B5 - 56 C	
100 LA B5R LB B5R		7.64	13.27	17.01	21.06	5.94	10.71	MPN 90 B5 - 140 TC	3.35
112 M B5R MC B5R		8.58	14.25	18.15	22.05	6.42		MPN 90 B5 - 180 TC	
								MPN 90 B5 - 180 TC ⁵⁾	
								MPN 100 B5R - 180 TC ⁶⁾	4.04
								MPN 100 B5R - 180 TC	11.8

1) Motor mounting position (see ch. 2b).

2) Values valid for HBZ brake motor.

3) No. 4 holes for each of the 2 B14 output flanges.

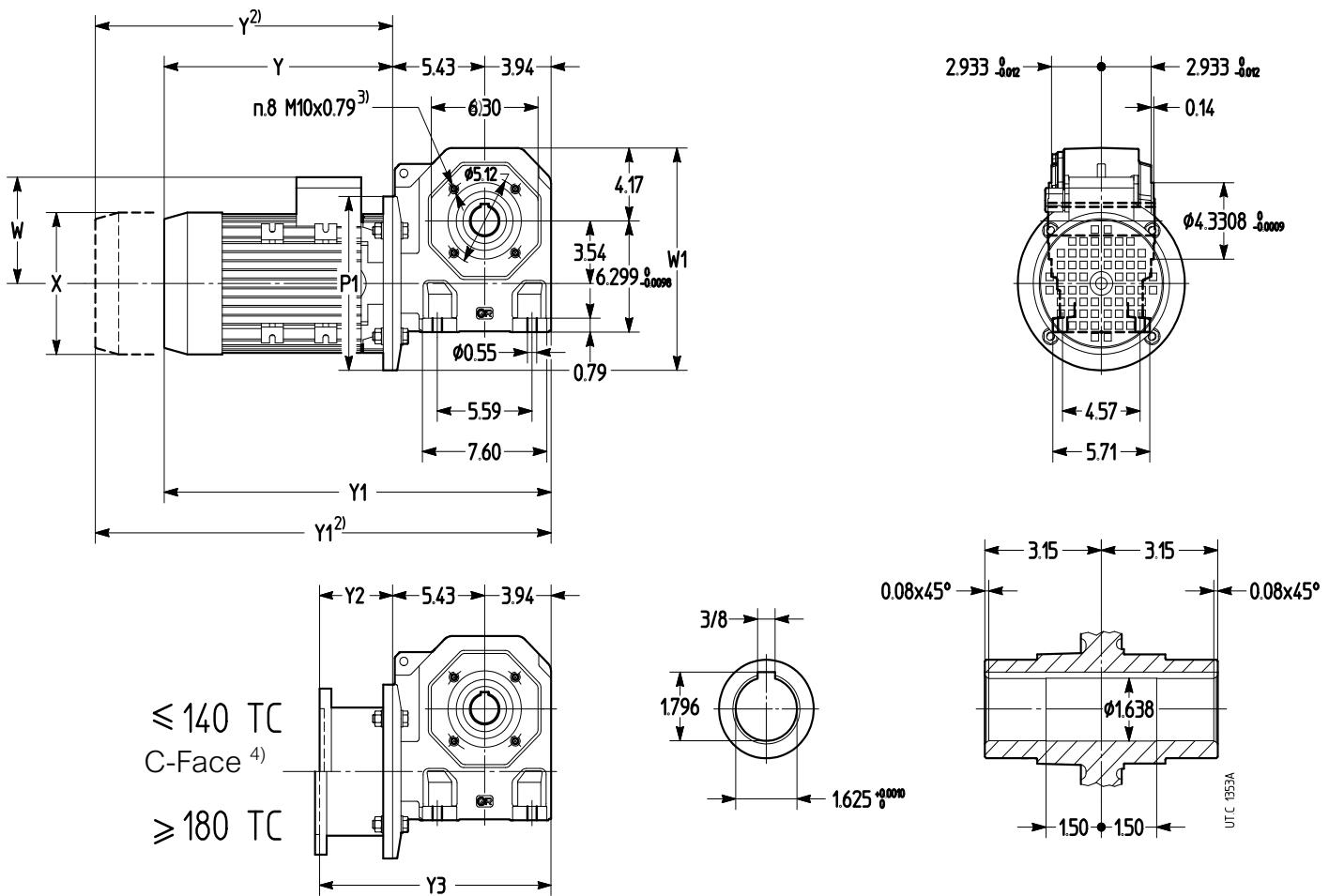
4) Available on request: for further dimensions and details see ch. 4.

5) Not available for 100LB 6 motor.

6) Not available for 112M 4 motor.

3.8 - Dimensions

Size **742**



Motor size		P1 \varnothing	X \varnothing \approx	Y \approx 2)	Y1 \approx 2)	W \approx	W1 \approx	NEMA C-Face adapter ⁴⁾		
1)								Y2	Y3	
90	S B5	200	6.93	11.3	14.41	20.67	23.78	5.55	11.65	MPN 90 B5 - 56 C
	L B5									MPN 90 B5 - 140 C
	LB B5									-
	LC B5									MPN 90 B5 - 180 C
100	LA B5	250	7.24	12.2	15.94	21.57	25.31	5.94	12.64	MPN 100 B5 - 180 C
	LB B5									MPN 100 B5 - 180 C ⁴⁾
112	M B5		8.58	13.23	17.13	22.6	26.5	6.42	12.64	MPN 100 B5 - 210 C ⁵⁾
	MC B5									MPN 100 B5 - 210 C ⁶⁾
132	S B5R		10.12	18.9	23.15	28.27	32.52	7.64	12.8	MPN 100 B5 - 210 C
	M B5R									MPN 100 B5 - 210 C
	MB B5R									-

1) Motor mounting position (see ch. 2b).

2) Values valid for HBZ brake motor.

3) No. 4 holes for each of the 2 B14 output flanges.

4) Available on request: for further dimensions and details see ch. 4

3.9 - Structural and operational details

Worm gear pair

Number of teeth – wormwheel z_2 and worm z_1 – axial module m_x , reference lead angle γ_m , static efficiency η_s of the worm gear pair.

i_N		Gear reducer size					
		118	225	325	430	535	742
6	z_2/z_1	18/3					
	m_x	2.2	–	–	–	–	–
	γ_m	22° 29'					
	η_s	0.71					
8.5	z_2/z_1	17/2	25/3	25/3	25/3	33/4	33/4
	m_x	2.3	2.2	2.8	3.4	3.5	4.5
	γ_m	15° 10'	22° 29'	22° 29'	22° 37'	28° 37'	28° 33'
	η_s	0.65	0.71	0.71	0.71	0.74	0.74
11.8	z_2/z_1	22/2	24/2	24/2	24/2	35/3	35/3
	m_x	1.8	2.3	2.8	3.5	3.3	4.2
	γ_m	13° 29'	15° 10'	15° 10'	15° 07'	19° 52'	20° 28'
	η_s	0.62	0.65	0.65	0.65	0.69	0.7
16	z_2/z_1	28/2	31/2	31/2	31/2	31/2	31/2
	m_x	1.5	1.8	2.3	2.9	3.7	4.7
	γ_m	11° 58'	13° 29'	13° 14'	13° 36'	14° 23'	14° 48'
	η_s	0.6	0.62	0.62	0.63	0.64	0.64
19	z_2/z_1	17/1	38/2	38/2	38/2	38/2	38/2
	m_x	2.3	1.5	1.9	2.4	3.1	3.9
	γ_m	7° 43'	11° 58'	11° 53'	12° 04'	12° 47'	13° 14'
	η_s	0.5	0.6	0.6	0.6	0.61	0.62
23.6	z_2/z_1	22/1	24/1	24/1	24/1	47/2	47/2
	m_x	1.9	2.3	2.8	3.5	2.5	3.2
	γ_m	6° 55'	7° 43'	7° 40'	7° 46'	11° 46'	12° 01'
	η_s	0.48	0.5	0.5	0.5	0.6	
30	z_2/z_1	28/1	30/1	30/1	30/1	30/1	30/1
	m_x	1.5	1.9	2.4	3	3.8	4.8
	γ_m	6° 00'	6° 55'	6° 52'	6° 58'	7° 21'	7° 34'
	η_s	0.45	0.48	0.48	0.48	0.5	0.5
37.5	z_2/z_1	35/1	38/1	38/1	37/1	37/1	37/1
	m_x	1.3	1.5	1.9	2.4	3.1	3.9
	γ_m	5° 14'	6° 00'	6° 00'	6° 03'	6° 25'	6° 38'
	η_s	0.42	0.45	0.45	0.45	0.46	0.47
47.5	z_2/z_1	44/1	47/1	47/1	47/1	47/1	47/1
	m_x	1	1.3	1.6	2	2.5	3.2
	γ_m	4° 30'	5° 14'	5° 10'	5° 16'	5° 54'	6° 02'
	η_s	0.38	0.42	0.42	0.42	0.44	0.45
60	z_2/z_1	—	58/1	58/1	58/1	58/1	58/1
	m_x	—	1	1.3	1.6	2.1	2.7
	γ_m	—	4° 30'	4° 25'	4° 32'	5° 07'	5° 15'
	η_s	—	0.38	0.38	0.38	0.41	0.42
75	z_2/z_1	—	—	73/1	73/1	73/1	73/1
	m_x	—	—	1	1.3	1.7	2.1
	γ_m	—	—	3° 43'	3° 50'	4° 21'	4° 27'
	η_s	—	—	0.34	0.35	0.38	0.38

Low speed shaft angular backlash

A rough guide for low speed shaft angular backlash is given in the table (the worm being held stationary). Values vary according to design and temperature.

- At a distance of 1 m from the low speed shaft centre, angular backlash in mm is obtained multiplying the table value by 1 000 (1 rad = 3438').

Gear reducer size	Angular backlash [rad] ¹⁾	
	min	max
118	0,0034	0,0132
225	0,0028	0,0112
325	0,0023	0,0090
430	0,0019	0,0075
535	0,0017	0,0067
742	0,0015	0,0056

3.9 - Structural and operational details

Efficiency η

Gear reducer efficiency η is given by P_2 / P_1 ratio (see ch. 3.7). The values obtained will be valid assuming normal working conditions, worm operating as driving member, proper lubrication, adequate running-in (see ch. 4), and a load near to the nominal value.

During the **initial working period** (about 50 hours) and generally at every cold start, efficiency will be lower (by about 12% for worms with $z_1 = 1$; 6% for worms with $z_1 = 2$ and 3% for worms with $z_1 = 3$).

«Static» efficiency η_s on starting (see table in the preceding section) is much lower than η (since «starting friction» must be overcome at speed 0); as speed picks up gradually, efficiency will rise correspondingly until the catalogue value is reached.

Inverse efficiency η_{inv} , – produced by the wormwheel as driver– is always less than η . It can be calculated approximately as follows:

$$\eta_{inv} \approx 2 - 1 / \eta; \quad \text{likewise:} \quad \eta_{s\ inv} \approx 2 - 1 / \eta_s$$

Irreversibility

The worm gearmotor is **dynamically irreversible** (that is, it ceases to turn the instant the wormshaft receives no further stimulus that would keep the worm itself in rotation e.g. motor torque, inertia from the worm, motor, flywheels, couplings, etc.) when $\eta < 0.5$ as η_{inv} then drops below 0.

This state becomes necessary wherever there is a **need for stopping and holding** the load, even without the aid of a brake. Where continuous vibration occurs, dynamic irreversibility may not be obtainable.

The gearmotor is **statically irreversible** (that is, rotation cannot be imparted by way of the low speed shaft) when $\eta_s < 0.5$.

This is a state **necessary to keep the load at standstill**; taking into account, however, that efficiency can increase with time spent in operation, it would be advisable to assume $\eta_s \leq 0.4$ ($\gamma_m < 5^\circ$).

Where continuous vibration occurs, static irreversibility may not be obtainable.

The gearmotor has **low static reversibility** (i.e. rotation may be imparted by way of the low speed shaft with high torque and/or vibration) when $0.5 < \eta_s \leq 0.6$ ($7^\circ 30' < \gamma_m \leq 12^\circ$).

The gearmotor has **complete static reversibility** (i.e. rotation may be imparted by way of the low speed shaft) when $\eta_s > 0.6$ ($\gamma_m > 12^\circ$).

This state is advisable where there is a **need for easy start-up of the gearmotor by way of the low speed shaft**.

Overloads

Since worm gear pairs are often subject to high static and dynamic overloads by dint of the fact that they are especially suited to bear them, the need arises – more so than with other gear pairs – to verify that such overloads will always remain lower than $T_{2\ max}$ (ch. 3.7).

Overloads are normally generated when one has:

- starting on full load (especially for high inertias and low transmission ratios), braking, shocks;
- irreversible gearmotors or gearmotors with low reversibility in which the worm-wheel becomes driver due to driven machine inertia;
- applied power higher than that required; other static or dynamic causes.

The following general observations on overloads are accompanied by some formulae for carrying out evaluations in certain typical instances.

Where no evaluation is possible, install safety devices which will keep values within $T_{2\ max}$.

Starting torque

When starting on full load (especially for high inertias and low transmission ratios) verify that $T_{2\ max}$ is equal to or greater than starting torque, by using the following formula:

$$T_{2\ start} = \left(\frac{T_{start}}{T_N} \cdot T_2 \text{ available} - T_2 \text{ required} \right) \frac{WK_R^2}{WK_R^2 + WK_0^2} + T_2 \text{ required}$$

where:

T_{start} is the motor starting torque (see ch.2);

T_N is the motor nominal torque (see ch. 2b);

T_2 available is output torque due to the motor's nominal power;

T_2 required is torque absorbed by the machine through work and frictions;

WK_0^2 is the moment of inertia (of mass) of the motor (see ch. 2b)

WK_R^2 is the external moment of inertia (of mass; coupling, driven machine) reflected to the motor shaft (see ch. 2b)

NOTE: When seeking to verify that starting torque is sufficiently high for starting, take into account efficiency η_s when evaluating T_2 available, and starting friction, if any, in evaluating M_2 required.

3.9 - Structural and operational details

Stopping machines with high kinetic energy (high moments of inertia combined with high speeds) with or without braking (braking applied to wormshaft, or use of brake motor)

Select a gear reducer with static reversibility ($\eta_{ls} > 0,5$); if using a brake motor, verify braking stress with the following formula:

$$\left(\frac{T_f}{\eta_{ls \text{ inv}}} \cdot i + T_2 \text{ required} \right) \frac{WK^2_R}{WK^2_R + WK^2_0} - T_2 \text{ required} \leq T_{2 \text{ max}}$$

where:

T_f is the braking torque setting (see cat. TX);

$\eta_{ls \text{ inv}}$ is static inverse efficiency (see previous heading);

for other symbols see above and ch.1.

Where selection of a statically reversible gearmotor is not possible (i.e. $\eta_s \leq 0,5$) slowing-down should be sufficiently gradual (avoiding application of excessive stress to the unit itself) as to ensure that:

$$0.373 \cdot WK^2_L \cdot \alpha_2 - T_2 \leq T_{2 \text{ max}}$$

where:

WK^2_L [lb ft²] is the moment of inertia (of mass) of the driven machine referred to the gear motors low speed shaft;

T_2 [N m] is torque absorbed by the machine through work and friction;

α_2 [rad/s²] is the low speed shaft's angular deceleration; this may be reduced by electric deceleration ramps, lowering of braking torque when braking systems are in use, etc.

α_2 may be arrived at theoretically (within broadly safe limits) or experimentally (by testing against stopping time and distance etc.). If a brake motor is in use, the following formula may be used for a safe evaluation of α_2 :

$$\alpha_2 = \frac{T_{\text{brake}}}{0.373 \cdot WK^2_L \cdot i}$$

in which the motor is presumed without load and subject to its braking torque setting T_{brake} [lbf in] (see cat. TX).

Operation with brake motor

Stating time ta and revolutions of motor φa_1

$$ta = \frac{(WK^2_0 + WK^2_R) \cdot n_1}{9,55 \left(T_{\text{start}} - \frac{T_2 \text{ required}}{i \cdot \eta} \right)} \text{ [s];} \quad \varphi a_1 = \frac{ta \cdot n_1}{19,1} \text{ [rad]}$$

Braking time tb and revolutions of motor φb_1

$$tb = \frac{(WK^2_0 + WK^2_R) \cdot n_1}{9,55 \left(Mb + \frac{T_2 \text{ required} \cdot \eta_{\text{inv}}}{i} \right)} \text{ [s];} \quad \varphi f_1 = \frac{tb \cdot n_1}{19,1} \text{ [rad]}$$

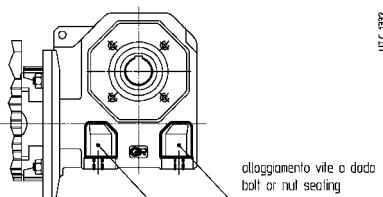
for symbols see above.

With the gear reducer run in and operating at normal running temperature — assuming a regular air-gap and ambient humidity and utilizing suitable electrical equipment — repetition of the braking action, as affected by variation in temperature of the brake and by the state of wear of friction surface, is approx $\pm 0,1 \cdot \varphi f_1$.

During warm-up (0,5 ÷ 2 h, small through to large sizes), braking times and distances tend to increase to the point of stabilizing at or around values corresponding to rated catalogue efficiency.

3.9 - Structural and operational details

Fixing bolt dimensions for gear reducer feet



Gear reducer size	ANSI B18.2.1 class 5	Bolt
		UNI 5737-88 UNI 5739-88 class 8.9
118	1/4 - 20 × 3/4	M 6 x 18
225	1/4 - 20 × 1	M 6 x 25
325	5/16 - 18 × 1 1/4	M 8 x 35
430	5/16 - 18 × 1 1/2	M 8 x 40
535	3/8 - 16 × 2	M10 x 50
742	7/16 - 14 × 2	M12 x 60

Maximum bending moment of flange MR

In case of assembly of motors supplied by the customer, verify that the static bending moment T_b generated by motor weight on the counter flange of gear reducer is lower than the value allowed T_{bmax} , stated in the table:

$$T_b \leq T_{bmax}$$

where:

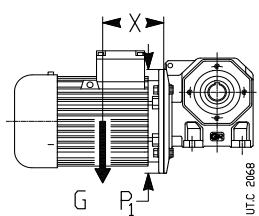
$$T_b = G \cdot X / 1000 \text{ [lbf in]}$$

G [lbf] motor weight

X [in] distance from motor center of gravity from fl ange surface

Very long and thin motors, though with bending moments within the prescribed limits, may generate anomalous vibrations during the operation. In these cases it is necessary to foresee a proper additional motor support (see motor specific documentation).

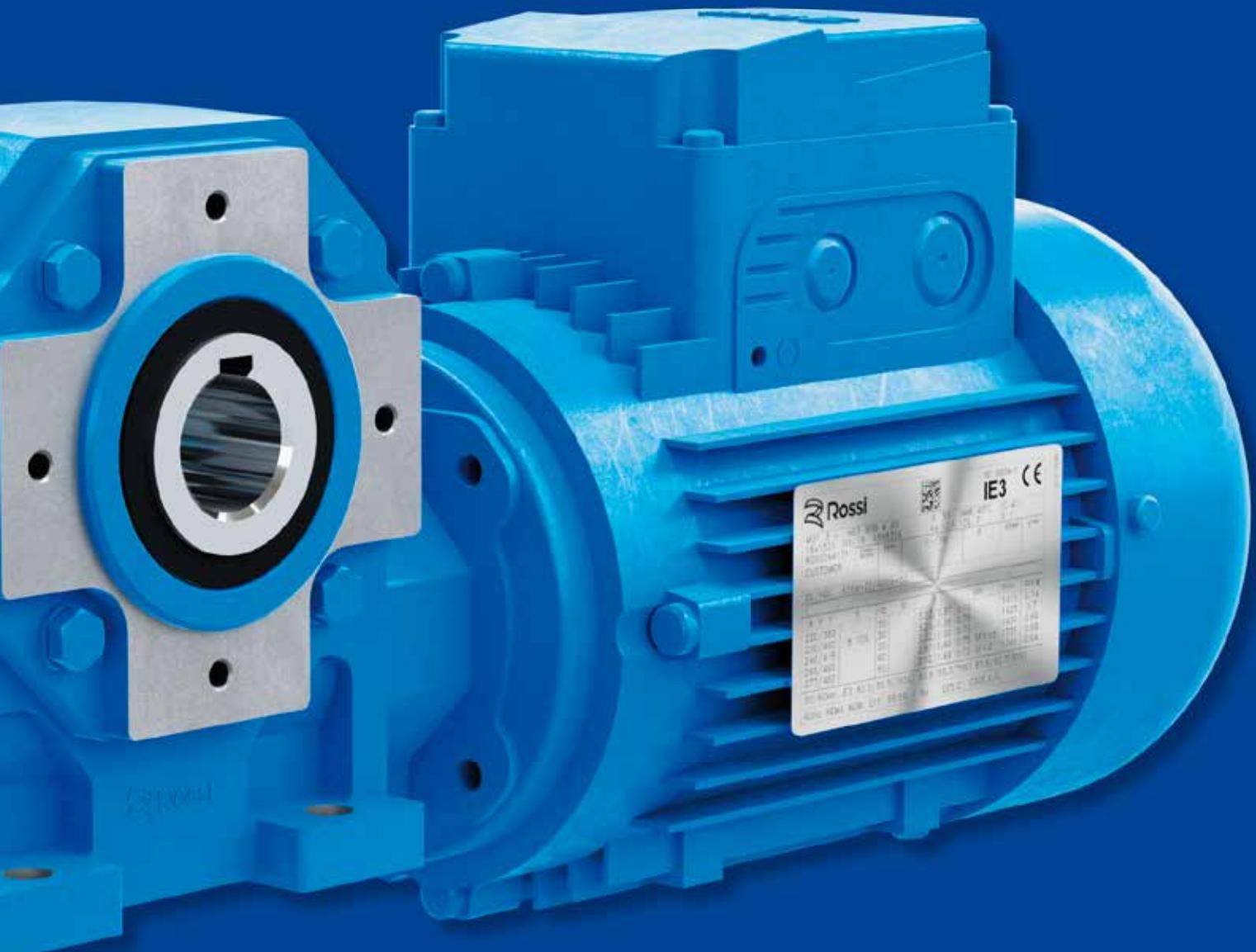
Loads higher than permissible loads may be present in dynamical applications where the gearmotor is subjected to translations, rotations or oscillations (e.g.: **shaft mounting arrangements**): consult us for the study of every specific case



Max allowable bending T_{bmax}

Gear reducer size	P ₁ Ø	T_{bmax} lbf in
118	90	500
225	90	500
325	105	800
430	200	2 500
535	200	4 000
742	200 250	4 000 8 000

Accessories and non-standard designs





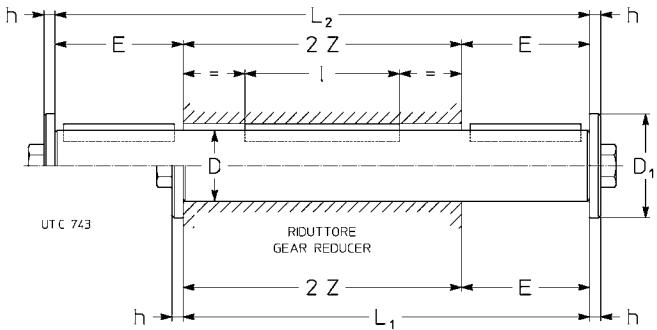
Section content

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4 - Accessories and non-standard designs

4.1 - Low speed shafts

The accessory is supplied fitted onto the gear reducer. If not differently stated, the standard mounting position for the low speed shaft end is on gear reducer right hand side – B3 mounting position – seen from motor side. For reverse mounting, specify in designation «**mounted on opposite side**».



Gear reducer size	U	V	Linguetta esterna External key	D₁	h	L₁	L₂	I	2 Z	Vite Bolt			Massa Mass	
	\varnothing		b x h x I							ANSI B18.2.1	Normale Stand.	Bisp. Doubl. extens.	lb	lb
118	0.75 $^{+0}_{-0.0005}$	1.19	3/16 x 3/16 x 1	1.1	0.16	3.98	5.17	1.5	2.8	1/4 - 20 x 3/4	0.46	0.62		
225	1 $^{+0}_{-0.0005}$	1.625	1/4 x 1/4 x 1 1/4	1.38	0.2	4.93	6.56	2.44	3.31	3/8 - 16 x 1	1.01	1.34		
325	1.125 $^{+0}_{-0.0005}$	1.625	1/4 x 1/4 x 1 1/4	1.38	0.2	5.48	7.11	2.44	3.86	3/8 - 16 x 1	1.46	1.9		
430	1.25 $^{+0}_{-0.0005}$	2.25	1/4 x 1/4 x 1 7/8	1.85	0.2	6.74	8.99	2.25	4.49	1/2 - 13 x 1 1/4	2.12	2.91		
535	1.375 $^{+0}_{-0.0005}$	2.25	3/16 x 3/16 x 1 13/16	1.85	0.2	7.6	9.85	2.37	5.35	1/2 - 13 x 1 1/4	2.98	3.91		
742	1.625 $^{+0}_{-0.0005}$	3.25	3/8 x 3/8 x 2 5/8	2.24	0.24	9.55	12.8	3.5	6.3	5/8 - 11 x 1 1/2	5.2	7		

The shoulder outer diameter of the part, or of spacer abutting with the gear reducer must be $(1,25 \div 1,4) \cdot D$.

Supplementary description when ordering by **designation: standard, or double extension low speed shaft**.

4.2 - Flange

B5 flange having clearance holes and spigot «recess».

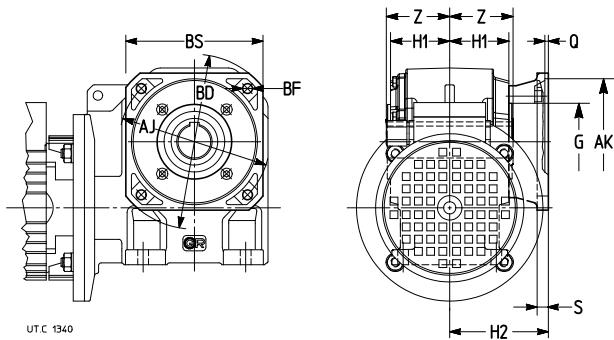
Available in two different options with different mating dimensions: **B5 flange** and **B5 flange Type B**.

The accessory is supplied fitted onto the gear reducer. If not differently stated, the standard mounting position is on gear reducer right hand side – B3 mounting position – seen from motor side. For reverse mounting, specify in designation «**mounted on opposite side**».

Locking adhesives are recommended both around threads and on mating surfaces.

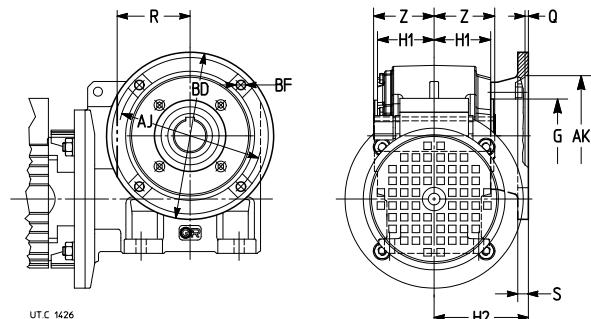
4 - Accessories and non-standard designs

B5 flange



Gear reducer size	BF Ø	G Ø	H1	H2	AJ Ø	AK Ø	BD Ø	Q	S	BS	Z	Mass
	in	in	in	in	in	in	in	in	in	in	in	lb
118	0.28	2.17	1.240 +0 -0.0098	2.677 +0 -0.0118	3.94	3.150 +0,0012 +0	4.72	0.16	0.39	3.74	1.4	1.1
225	0.28	2.44	1.476 +0 -0.0098	2.913 +0 -0.0118	3.94	3.150 +0,0012 +0	4.72	0.16	0.39	3.74	1.65	1.1
325	0.37	2.68	1.752 +0 -0.0098	3.268 +0 -0.0138	4.53	3.740 +0,0014 +0	5.51	0.16	0.43	4.33	1.93	1.8
430	0.37	3.35	2.087 +0 -0.0118	3.307 +0 -0.0138	5.12	4.331 +0,0014 +0	6.3	0.18	0.47	4.92	2.24	2.2
535	0.45	3.15	2.5 +0 -0.0118	4.134 +0 -0.0138	6.50	5.118 +0,0016 +0	7.87	0.18	0.55	5.98	2.68	4
742	0.55	4.33	2.933 +0 -0.0118	4.606 +0 -0.0138	8.47	7.087 +0,0016 +0	9.84	0.2	0.63	7.72	3.15	7

B5 flange type B



Gear reducer size	BF Ø	G Ø	H1	H2	AJ Ø	AK Ø	BD Ø	Q	R	S	Z	Mass
	in	in	in	in	in	in	in	in	in	in	in	lb
118	0.37	2.17	1.240 +0 -0.0098	2.835 +0 -0.0118	3.43	2.362 +0,0012 +0	4.33	0.2	-	0.35	1.4	1.8
225	0.45	2.44	1.476 +0 -0.0098	3.425 +0 -0.0138	3.54	2.756 +0,0012 +0	4.92	0.2	-	0.39	1.65	2.2
325	0.45	2.68	1.752 +0 -0.0098	3.346 +0 -0.0138	5.91	4.528 +0,0014 +0	7.09	0.2	3.15	0.43	1.93	3.7
430	0.55	3.35	2.087 +0 -0.0118	4.016 +0 -0.0138	6.5	5.118 +0,0016 +0	7.87	0.2	3.58	0.47	2.24	5.3
535	0.55	3.15	2.5 +0 -0.0118	4.409 +0 -0.0138	6.93	5.984 +0,0016 +0	8.27	0.24	-	0.55	2.68	6.4
742	0.55	4.33	2.933 +0 -0.0118	5.276 +0 -0.0157	9.06	6.693 +0,0016 +0	11.02	0.24	4.76	0.63	3.15	12.8

Supplementary description when ordering by **designation: flange B5 or B5 flange type B**.

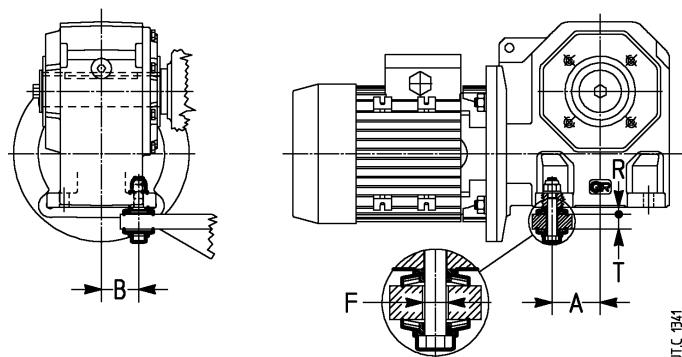
In case of separate order from the gear reducer's one, the accessory designation must include the catalog and gear reducers size data.

4.3 - Shaft-mounting arrangements

Reaction bolt using disc springs

Semi-flexible and economical reaction arrangement, with bolt using disc springs.

IMPORTANT: Comply with recommendations at ch.12 for shaft mounting.



Gear red. size	A	B	Bolt	Disc spring	T	F _Ø	R	M ₂ ≈
			UNI 5737-88	DIN 2093				N m
118	1.28	0.91	M6 × 40	A 18 n.2	0.31 ± 0.39	0.31	0.19	-
225	1.28	1.14	M6 × 40	A 18 n.2	0.31 ± 0.39	0.31	0.19	-
325	1.48	1.34	M8 × 55	A 25 n.2	0.39 ± 0.55	0.43	0.26	-
430	1.81	1.63	M8 × 55	A 25 n.2	0.39 ± 0.55	0.43	0.26	-
535	2.17	1.97	M12 × 70*	A 35,5 n.2	0.55 ± 0.67	0.79	0.35	2 800
742	2.8	2.28	M12 × 90	A 35,5 n.3	0.71 ± 0.98	0.79	0.53	5 300

1) For higher M₂ values, utilize 2 reaction bolts or the torque arm (see below).

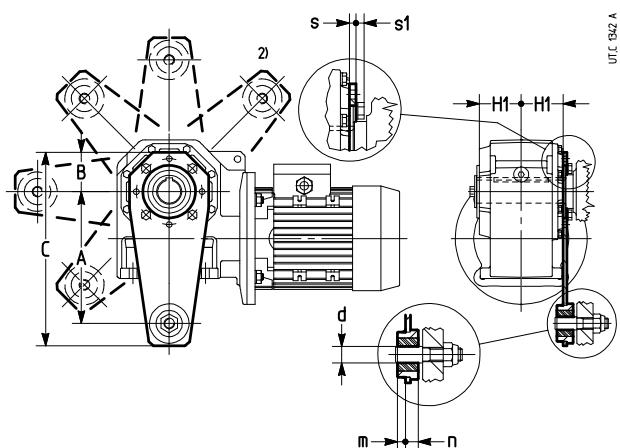
* Modified bolt.

Supplementary description when ordering by **designation: reaction bolt using disc springs.**

Torque arm

Reaction arrangement using torque arm, fitted onto B14 flange, with plastic damping bush (not present for sizes 118, 225). The accessory, including fixing bolts, is supplied not assembled. Fitting towards motor is not possible.

IMPORTANT: comply with recommendations at ch. for shaft mounting.



Gear red. size	A	B	C	d Ø	H1	m	n Ø	s	s1	M ₂ ≈
118	3.94	1.77	6.18	0.315 ^{+0,0035¹⁾}	1.24 ⁺⁰ _{-0,0098}	0.2	0.35	0.16	0.19	95
225	3.94	1.77	6.18	0.315 ^{+0,0035¹⁾}	1.476 ⁺⁰ _{-0,0098}	0.2	0.35	0.16	0.19	95
325	5.91	2.07	9.06	0.394 ^{+0,0035}	1.752 ⁺⁰ _{-0,0098}	0.28	0.51	0.24	0.22	150
430	7.87	2.36	11.57	0.787 ^{+0,0051}	2.087 ⁺⁰ _{-0,0118}	0.37	0.61	0.24	0.22	180
535	7.87	2.36	11.57	0.787 ^{+0,0051}	2.5 ⁺⁰ _{-0,0118}	0.37	0.61	0.24	0.3	335
742	9.84	3.15	14.33	0.787 ^{+0,0051}	2.933 ⁺⁰ _{-0,0118}	0.37	0.61	0.24	0.36	670

1) Plastic damping bush not present.

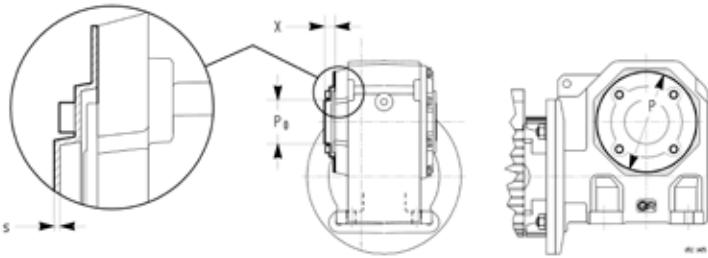
2) Position not possible for size 430.

Supplementary description when ordering by **designation: torque arm.**

4.4 - Hollow low speed shaft **STANDARDFIT** protection

Protection hollow low speed shaft free area, made of plastic (polypropilene PP material color black)

The accessory is supplied disassembled and complete with fastening screws. We recommend the use of locking adhesive on the screws.



Gear reducer size	P	P₀	X	S	Screws	Tightening
	Ø	Ø			UNI 5931	2) lbf in
118, 225	3.54	1.89	0.81	0.059 ^{+0,0012} ₊₀	M5×14	13,5
325	4.13	1.97	0.81	0.063 ^{+0,0012} ₊₀	M6×18	25
430	4.72	2.40	0.94	0.067 ^{+0,0012} ₊₀	M6×18	25
535¹⁾	4.72	2.40	0.94	0.067 ^{+0,0012} ₊₀	M8×20	56
742	6.30	3.07	1.08	0.071 ^{+0,0012} ₊₀	M10×20	109

1) For size 535, gear reducer P dimensions is equal to 5.12 in.

2) Tightening torque.

Non standard design code for designation:

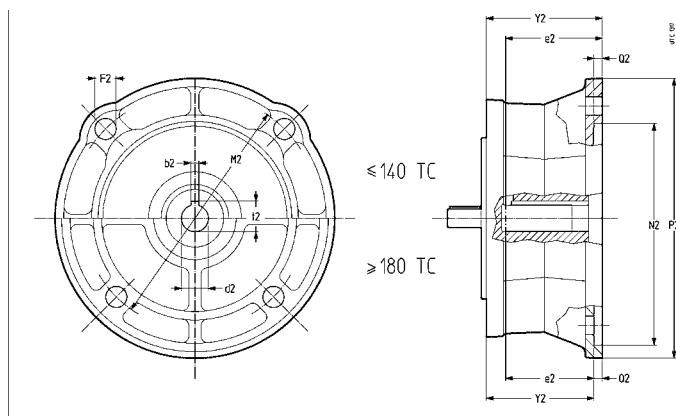
Hollow low speed shaft **STANDARDFIT** protection

In case of separate order from the gear reducer's one, the accessory designation must include the catalog and gear reducers size data.

4.5 - NEMA C-Face adapter

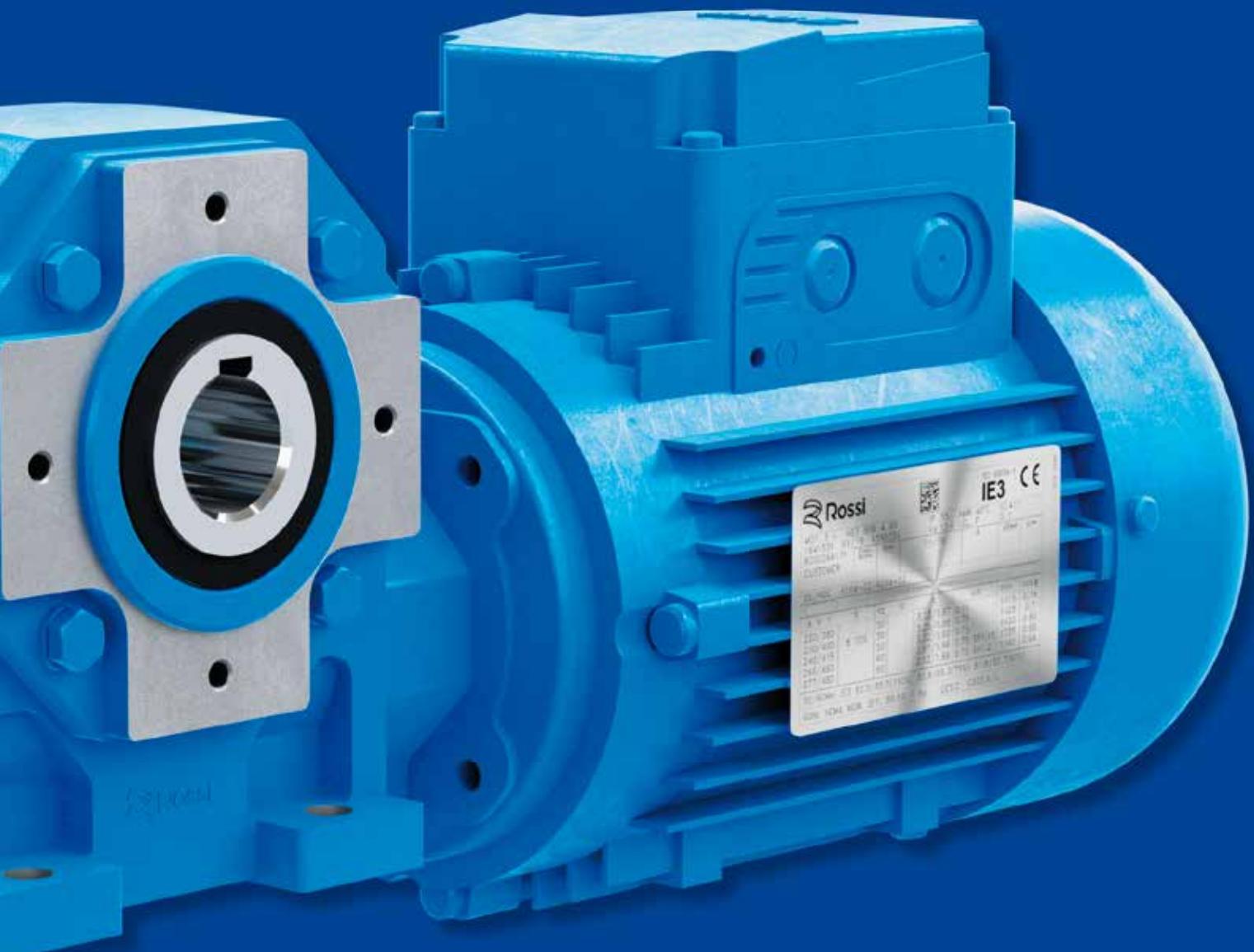
Cast iron casing, device transforming gearmotor IEC input side into NEMA C-Face mating dimensions (see ch. 10 for possible combinations).

Designation code for ordering and dimensions as per table below.



Designation code	NEMA C-Face input side frame size	U1 Ø	V1	S1	t1	BF1 Ø	AJ1 Ø	AK1 Ø	BD1 Ø	Q1	Y2	Weight lb
MPN 63 B14 - 56 C	56 C	0.625	2.06	0.188	0.709	0.43	5.875	4.5	6.5	0.2	2.7	5.6
MPN 71 B14 - 56 C												5.9
MPN 80 B5 - 56 C												9.6
MPN 90 B5 - 56 C												9.8
MPN 90 B5 - 140 TC	140 TC	0.875	2.12	0.188	0.964	0.43	5.875	4.5	6.5	0.2	2.7	9.6
MPN 90 B5R - 140 TC												9.4
MPN 90 B5 - 180 TC	180 TC	1.125	2.62	0.25	1.241	0.56	7.25	8.5	9	0.22	3.35	17.1
MPN 90 B5R - 180 TC												16.9
MPN 100 B5 - 180 TC	210 TC	1.375	3.12	0.312	1.518	0.56	7.25	8.5	9	0.22	4.04	20.5
MPN 100 B5 - 210 TC												23.9
MPN 100 B5R - 210 TC												20.3

Installation and maintenance





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5 -Installation and maintenance

5.1 - General

Be sure that the structure on which gearmotor is fitted is plane, levelled and sufficiently dimensioned in order to assure fitting stability and vibration absence, keeping in mind all transmitted forces due to the masses, to the torque, to the radial and axial loads.

Position the gearmotor so as to allow a free passage of air for cooling both gear reducer and motor (especially at motor fan side).

Avoid: any obstruction to the air-flow; heat sources near the gear reducer that might affect the temperature of cooling-air and of gear motor for radiation; insufficient air recycle or any other factor hindering the steady dissipation of heat.

Mount the gearmotor so as not to receive vibrations.

When external loads are present use pins or locking blocks, if necessary.

When fitting gear reducer and machine and/or gear reducer and eventual flange **B5** it is recommended to use **locking adhesives** such as LOCTITE on the fastening screws (also on flange mating surfaces).

For outdoor installation or in a hostile environment protect the gear motor with anticorrosion paint. Added protection may be afforded by water-repellent grease (especially around the rotary seating of seal rings and the accessible zones of shaft end).

Gearmotors should be protected wherever possible, and by whatever appropriate means, from solar radiation and extremes of weather; weather protection **becomes essential** for **B6**, **V5** and **V6** mounting positions.

For ambient temperatures greater than 40 °C or less than 0 °C, consult us.

Before wiring up the gearmotor, make sure that motor voltage corresponds to input voltage. If the direction of rotation is not as desired, invert two phases at the terminals.

If overloads are imposed for long periods of time, or if shocks or danger of jamming are envisaged, then motor-protections, electronic torque limiters, safety couplings, control units or other suitable devices should be fitted.

Where duty cycles involve a high number of starts on load, it is advisable to utilize **thermal probes** (fitted on the wiring) for motor protection; a thermal overload relay is unsuitable since its threshold must be set higher than the motor's nominal current rating.

Use varistors to limit voltage peaks due to contactors.

Warning! Bearing life, good shaft and coupling running depend on alignment precision between the shafts. Carefully align the gearmotor with the driven machine (with the aid of shims if need be), interposing flexible couplings whenever possible.

Whenever a leakage of lubricant could cause heavy damages, increase the frequency of inspections and/or envisage appropriate control devices (e.g.: remote oil level gauge, lubricant for food industry, etc.).

In polluting surroundings, take suitable precautions against lubricant contamination through seal rings or other.

Gearmotor should not be put into service before it has been incorporated on a machine which is conform to 98/37/EC directive.

For brake or non-standard motors, consult us for specific documentation.

Gear reducer size	Hollow low speed shaft diameter	Shaft recommended tolerances		
		ØU	Load cl. I	Load cl. II, III
118	0.75	+0.0010 +0	+0.0003 +0.0002	+0.0005 -0.0003
225	1	+0.0010 +0	+0.0004 +0	+0.0006 -0.0003
325	1.125	+0.0010 +0	+0.0004 +0	+0.0006 -0.0003
430	1.25	+0.0010 +0	+0.0004 +0	+0.0006 -0.0003
535	1.375	+0.0010 +0	+0.0004 +0.0002	+0.0007 -0.0001
742	1.625	+0.0010 +0	+0.0004 +0.0002	+0.0007 -0.0001

5 -Installation and maintenance

5.2 - Machine shaft

For the machine shaft, where the hollow shaft of the gear reducer is to be keyed, the following tolerances are recommended (according to load classification): For complete hollow low speed shaft dimensions see ch.

Important: the shoulder diameter of the machine shaft end abutting with the gear reducer must be at least $(1.18 \pm 1.25) \cdot U$.

Before mounting, clean mating surfaces thoroughly and lubricate against seizure and fretting corrosion. Installing and removal operations should be carried out with **pullers** and **jacking screws**.

Fitting of components to shaft ends

For the **bore** of **parts** keyed to the low speed shaft end, the following **tolerances** are **recommended** (according to load classification):

Gear reducer size	Low speed shaft diameter	Bore recommended tolerances		
		ØU	Load cl. I	Load cl. II, III
118	0.75	+0 -0.0005	+0.0006 +0	+0.0008 -0.0005
225	1	+0 -0.0005	+0.0016 +0	+0.0010 -0.0006
325	1.125	+0 -0.0005	+0.0016 +0	+0.0010 -0.0006
430	1.25	+0 -0.0005	+0.0016 +0	+0.0010 -0.0006
535	1.375	+0 -0.0005	+0.0020 +0	+0.0013 -0.0007
742	1.625	+0 -0.0005	+0.0020 +0	+0.0013 -0.0007

5.3 - Shaft-mounting arrangements

IMPORTANT. When shaft mounted, the gearmotor must be supported both axially and radially by the shaft end of the driven machine, as well as anchored against rotation only, by means of a reaction having **freedom of axial movement** and sufficient **clearance in its couplings** to permit minor oscillations – always in evidence – without provoking dangerous overloads on the actual gearmotor. Pivots and components subject to sliding have to be properly lubricated; we recommend the use of a locking adhesive such as LOCTITE 601 when fitting the bolts.

5.4 - IEC frame motor mounting or replacement

For IEC frame motor mounting simply observe the following instructions:

- ensure that the mating surfaces are machined under standard rating (IEC 72.1; UNEL 13501-69; DIN 42955) at least;
- clean surfaces to be fitted, thoroughly;
- check and, if necessary, lower the parallel key so as to leave a clearance of 0.004 - 0.008 in (01 - 0.2 mm) between its tip and the bottom of the keyway; if shaft keyway is without end, lock the key with a pin;
- lubricate surfaces to be fitted against fretting corrosion.

For other details regarding motor mounting, see specific information and/or consult us.

The replacement of a motor supplied by us with an IEC frame motor 1) of the same power supplied by the Customer is possible only for motors stated in ch. 9, in mounting positions B5 or B14.

However, if need be and accepting a reduced machine duty cycle, it is possible to replace the motors in mounting position B5*, B14* (i.e.: with power of motor power-to-size correspondence not according to standard), B5R and B14R with motors standardized to IEC of smaller power and size, if possible, having mating dimensions as stated in ch. ...

1) NEMA C-Face motors may be fitted in combination with an adapter device supplied as accessory (see ch. 13 for dimensions and possible combination).

6 -Technical formulae

Main formulas concerning mechanical drives, according to the Technical System and International Unit System (SI).

Size	With Technical System units	With SI units
starting or stopping time as a function of an acceleration or deceleration, of a starting or braking torque	$t = \frac{v}{a}$ [s] $t = \frac{Gd^2 \cdot n}{375 \cdot M}$ [s]	$t = \frac{J \cdot \omega}{M}$ [s]
velocity in rotary motion	$v = \frac{\pi \cdot d \cdot n}{60} = \frac{d \cdot n}{19,1}$ [m/s]	$v = \omega \cdot r$ [m/s]
speed	$n = \frac{60 \cdot v}{\pi \cdot d} = \frac{19,1 \cdot v}{d}$ [min ⁻¹]	$\omega = \frac{v}{r}$ [rad/s]
acceleration or deceleration as a function of starting or stopping time		$a = \frac{v}{t}$ [m/s ²]
angular acceleration or deceleration as a function of a starting or stopping time, of a starting or braking torque	$\alpha = \frac{n}{9,55 \cdot t}$ [rad/s ²] $\alpha = \frac{39,2 \cdot M}{Gd^2}$ [rad/s ²]	$\alpha = \frac{\omega}{t}$ [rad/s ²] $\alpha = \frac{M}{J}$ [rad/s ²]
starting or stopping distance as a function of a starting or stopping time, of a starting or braking velocity	$s = \frac{a \cdot t^2}{2}$ [m]	$s = \frac{v \cdot t}{2}$ [m]
starting or stopping angle as a function of an angular acceleration or deceleration, of a final or initial angular velocity	$\varphi = \frac{n \cdot t}{19,1}$ [rad]	$\varphi = \frac{\omega \cdot t}{2}$ [rad]
mass	$m = \frac{G}{g}$ [$\frac{\text{kgf s}^2}{\text{m}}$] m is the unit of mass [kg]	$G = m \cdot g$ [N]
weight (weight force)	G is the unit of weight (weight force) [kgf]	
force in vertical (lifting), horizontal, inclined motion of translation (μ = coefficient of friction; φ = angle of inclination)	$F = G$ [kgf] $F = \mu \cdot G$ [kgf] $F = G (\mu \cdot \cos \varphi + \sin \varphi)$ [kgf]	$F = m \cdot g$ [N] $F = \mu \cdot m \cdot g$ [N] $F = m \cdot g (\mu \cdot \cos \varphi + \sin \varphi)$ [N]
dynamic moment Gd^2 , moment of inertia J due to a motion of translation (numerically $J = \frac{Gd^2}{4}$)	$Gd^2 = \frac{365 \cdot G \cdot v^2}{n^2}$ [kgf m ²]	$J = \frac{m \cdot v^2}{\omega^2}$ [kg m ²]
torque as a function of a force, of a dynamic moment or of a moment of inertia, of a power	$M = \frac{F \cdot d}{2}$ [kgf m] $M = \frac{Gd^2 \cdot n}{375 \cdot t}$ [kgf m] $M = \frac{716 \cdot P}{n}$ [kgf m]	$M = F \cdot r$ [N m] $M = \frac{J \cdot \omega}{t}$ [N m] $M = \frac{P}{\omega}$ [N m]
work, energy in motion of translation, in rotary motion	$W = \frac{G \cdot v^2}{19,6}$ [kgf m] $W = \frac{Gd^2 \cdot n^2}{7160}$ [kgf m]	$W = \frac{m \cdot v^2}{2}$ [J] $W = \frac{J \cdot \omega^2}{2}$ [J]
power in motion of translation, in rotary motion	$P = \frac{F \cdot v}{75}$ [CV] $P = \frac{M \cdot n}{716}$ [CV]	$P = F \cdot v$ [W] $P = M \cdot \omega$ [W]
power available at the shaft of a single-phase motor ($\cos \varphi$ = power factor)	$P = \frac{U \cdot I \cdot \eta \cdot \cos \varphi}{736}$ [CV]	$P = U \cdot I \cdot \eta \cdot \cos \varphi$ [W]
power available at the shaft of a three-phase motor	$P = \frac{U \cdot I \cdot \eta \cdot \cos \varphi}{425}$ [CV]	$P = 1,73 \cdot U \cdot I \cdot \eta \cdot \cos \varphi$ [W]

Note. Acceleration or deceleration are understood constant; motion of translation and rotary motion are understood rectilinear and circular respectively.



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